

**ORDER**

U.S. DEPARTMENT OF TRANSPORTATION  
FEDERAL AVIATION ADMINISTRATION

**8260.40A**

**12/5/95**

**SUBJ: FLIGHT MANAGEMENT SYSTEM (FMS) INSTRUMENT PROCEDURES DEVELOPMENT**

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- 1. PURPOSE.** This order provides criteria for establishing instrument nonprecision area navigation (RNAV) approach, transition to instrument landing system (ILS) precision final approach, departure and missed approach procedures for FMS-equipped aircraft, in conjunction with FAA Handbook 8260.3B, United States Standard for Terminal Instrument Procedures (TERPS), and FAA Order 8260.36, Civil Utilization of Microwave Landing System (MLS).
- 2. DISTRIBUTION.** This order is distributed to the branch level in the offices of System Safety; Aviation Policy and Plans; Air Traffic Systems Development; Aviation Research; Communication, Navigation, and Surveillance Systems; Airport Safety and Standards; Aviation System Standards; Air Traffic Rules and Procedures; and in the Services of Flight Standards, and Airway Facilities; to the National Airway Systems Engineering Division; to the National Flight Procedures Office; to the Regulatory Standards and Compliance Division at the Mike Monroney Aeronautical Center; to the branch level in the regional Flight Standards, Air Traffic, Airway Facilities, and Airports divisions; to all Flight Inspection Area Offices, and the International Flight Inspection Office; to the Europe, Africa, and Middle East International Area Office; to all Flight Standards District Offices; to all Airway Facilities Sectors, and Sector Field Offices; and to all addresses on special distribution lists ZVN-826, ZVS-827, and ZAT-423.
- 3. CANCELLATION.** Order 8260.40, Flight Management System (FMS) Instrument Procedure Development, dated June 10, 1994, is canceled.
- 4. DEFINITIONS.**
  - a. Approach Operations.** That portion of flight conducted on charted Instrument Approach Procedures (IAP's) commencing at the initial approach waypoint (IAWP) and concluding at landing or the missed approach holding waypoint (MAHWP). All FMS instrument approaches shall be called up from a data base contained within the FMS itself.
  - b. Departure End of Runway (DER).** The end of the takeoff run available.
  - c. En Route Operations.** That portion of flight conducted on charted VOR routes designated as high or low altitude routes (Jet or Victor) or direct point-to-point operations between defined waypoints.

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**Initiated By:** AFS-400

**d. Instrument Approach Waypoints.** Geographical positions, specified in latitude/longitude, used in defining FMS instrument approach procedures. An FMS approach may include some or all of the following waypoints; feeder waypoint (FWP), IAWP, intermediate waypoint (IWP), final approach waypoint (FAWP), missed approach waypoint (MAWP), runway waypoint (RWP) and MAHWP.

**e. Reference Waypoint.** A waypoint of known location used to geodetically compute the location of another waypoint.

**f. Roll Anticipation Distance (RAD).** The distance traveled by the aircraft while rolling to the bank angle required for a turn.

**g. Runway Waypoint (RWP).** A waypoint located on the runway centerline at the runway threshold.

**h. Takeoff Run Available (TORA).** The runway length declared available for the ground run of an airplane takeoff.

**i. Takeoff Waypoint (TOWP).** A waypoint located on runway centerline at the beginning of TORA.

**j. Terminal Operations.** That portion of flight conducted on charted Standard Instrument Departures (SID's), on charted Standard Terminal Arrivals (STAR's), or other flight operations between the last en route waypoint and the IAWP (i.e., feeder routes).

**k. Turn Anticipation.** The capability of FMS to determine the point along a course, prior to a fly-by waypoint, where a turn is initiated to provide a smooth path to intercept the succeeding course. Turn distance includes roll anticipation distance as well as the distance necessary to make the required turn.

**l. Waypoint (WP).** A predetermined geographical position used for route definition and/or progress reporting purposes that is defined by latitude/longitude. A fly-by waypoint requires the use of turn anticipation to avoid overshoot of the next flight segment. A fly-over waypoint precludes any turn until the waypoint is overflown and is followed by an intercept maneuver of the next flight segment.

**m. Waypoint Displacement Area.** The rectangular area formed around and centered on the plotted position of the waypoint. This describes the region within which the aircraft could be placed when attempting to fly over the waypoint considering all error components. Its dimensions are plus-and-minus the appropriate alongtrack (ATRK) and crosstrack (XTRK) fix displacement tolerance values found in table 1.

## SECTION 1. GENERAL CRITERIA

### 5. GENERAL CRITERIA.

a. Use of FMS procedures developed in accordance with these criteria shall be limited to aircraft qualifying for the /G equipment suffix. The Airman's Information Manual defines /G-equipped aircraft as those possessing a RNAV capability with a FMS and which have received a "Special Aircraft and Aircrew Authorization" by the Technical Programs Division of the FAA Flight Standards Service. Specific aircraft equipment requirements to qualify for the /G designation and, hence, for procedures developed using the criteria contained herein are:

(1) At least one FMS which meets the specifications of FAA Advisory Circular (AC) 25-15, approval of Flight Management Systems in Transport Category Airplanes, and AC 20-130, Airworthiness Approval of Multi-Sensor Navigation Systems for Use in the U.S. National Airspace System (NAS) and Alaska, or equivalent criteria.

(2) A flight director and autoflight control system capable of following the designated lateral FMS flightpath.

(3) Dual or triple inertial reference units (IRU) updated by DME/DME or GPS with verification of facility performance and suitable geometry for the route or procedure.

(4) Any applicable route or procedure to be flown must be automatically loaded into the FMS flight plan from the FMS data base and verified by the flightcrew.

b. Missed approach (MA) and departure procedures should follow the same route. Departure procedures will overlie FAR 121.189 routes to the maximum extent possible.

c. Do not use this order for instrument procedure altitudes above 15,000 feet MSL.

**6. GENERAL PROCEDURE CONSTRUCTION CRITERIA.** General FMS procedural construction requirements are as follows:

**a. Waypoints.** Except in the case of an ILS final approach segment, a WP shall be used to identify the beginning point and ending point of each segment in a FMS procedure. WP's shall also be established at holding fixes or at other points of operational benefit, such as waypoints associated with altitude and/or airspeed restrictions. (ILS final approach segment is as defined in TERPS, chapter 9, paragraph 930, or Order 8260.36, paragraph 16, for new ILS installations.) The following waypoint guidelines apply:

(1) Fly-by waypoints should be used whenever possible.

(2) Fly-over waypoints should only be used when operationally necessary; e.g., to insure lateral avoidance of an obstacle on departure, to insure over fly of the MAWP. Fly-over waypoints shall not be used for the IAWP, IWP and the FAWP. Table 1 shows which waypoints may be designated as fly-over.

(3) Waypoint displacement tolerances are associated with each waypoint. Displacement tolerance areas for consecutive waypoints shall not overlap. Table 1 contains a summary of waypoint displacement tolerances for each type of waypoint.

(4) Procedures should be designed using the fewest number of waypoints possible.

(5) Waypoints shall be designated where course, speed or altitude changes occur.

(6) Procedures shall be designed using seamless path construction and there shall not be any route gaps or discontinuities.

(7) Each WP shall be defined by latitude and longitude in degrees, minutes, and seconds and shall be developed to the nearest hundredth of a second.

**b. Segments.** FMS RNAV segments begin and end at a WP.

(1) The segment area considered for obstacle clearance begins at the earliest point of the beginning WP displacement area and, except for the final approach segment, ends at the plotted position of the next WP.

(2) Segment length, except for the final approach segment, is based on the distance between the plotted positions of the WP's defining the segment. Final approach segment length is defined in the appropriate section.

(3) Minimum segment lengths are determined using the following guidelines:

(a) Unless otherwise stated, minimum segment lengths are functions of waypoint type, aircraft speed and amount of course change at the waypoint and are determined from values contained in table 2 (fly-by waypoints) and table 3 (fly-over waypoints). Figures 1A, 1B, 1C, 1D, and 1E show how to apply tables 2 and 3 to various combinations of waypoint types.

(b) Table 4 contains speed applicability for the various instrument procedure segments, except the final approach segment. Table 4 is used as an entry key to obtain the appropriate data from tables 2, 3, and 5. Table 6 contains the minimum FMS nonprecision final approach segment length based on the amount of turn at the FAWP. If it is necessary to restrict airspeed to values less than shown in table 4, select the appropriate speed from tables 2, 3, and 5 and annotate the procedure accordingly. An approach segment shall not be designed using a higher airspeed than the preceding segment; e.g., the initial segment designed using 160 KIAS while the intermediate segment designed using 220 KIAS.

(c) For consecutive fly-by waypoints with turns in the same direction, the minimum turn distance from table 2 may be reduced by the roll anticipation distance from table 5. (See figure 1E.)

(d) In no case will a segment length be less than the sum of the ATRK waypoint displacement tolerances for the respective waypoints. See table 1 for ATRK waypoint displacement tolerances for the various type waypoints.

(e) The following example illustrates these concepts:

**Example:** Given the FMS approach as shown in figure 2, determine the minimum length of each segment. Every waypoint is fly-by and the maximum altitude on the approach is 7,000 feet.

**En Route Segment (En Route WP - FWP).** Since FMS navigation is seamless, the angle of turn, if any, at the en route WP must be known before the minimum distance could be determined.

**Feeder Segment (FWP - IAWP).** Since this is a feeder segment and the maximum altitude is less than 10,000 feet MSL, table 4 shows that the 250 KIAS column in table 2 is to be used. Since no course change takes place at the FWP, only the 90-degree course change at the IAWP will figure in the minimum segment length determination. From table 2 for 250 KIAS and 90-degree course change, the minimum turn distance is 4.91 NM. For this example, this is also the minimum segment length. Remember that the segment length can be no shorter than the sum of the ATRK waypoint displacement tolerances. From table 1, the ATRK waypoint displacement tolerance is 1.7 NM at the FWP and

.3 NM at the IAWP. Summing these results in 2.0 NM. Therefore, the 4.91 NM as previously determined is the minimum feeder route length for this example.

**Initial Segment (IAWP-IWP).** From table 4, the 220 KIAS column of table 2 is to be used for the initial segment. Since there is a course change at both the IAWP and the IWP, two minimum turn distances must be determined. First, from table 2 for 220 KIAS and the 90-degree course change at the IAWP, the minimum turn distance is 4.06 NM. Second, from table 2 for 220 KIAS and the 60-degree course change at the IWP, the minimum turn distance is 2.63 NM. Adding these two distances together results in a minimum initial segment length of 6.69 NM.

**Intermediate Segment (IWP - FAWP).** From table 4, the 175 KIAS column of table 2 is to be used for the intermediate segment. Again, course changes take place at both waypoints, thus two minimum turn distances will be determined. From table 2 for 175 KIAS and the 60-degree course change at the IWP, the minimum turn distance is 1.93 NM. Notice, however, that the turns at the IWP and the FAWP are in the same direction, so the RAD may be subtracted from the minimum turn distance. From table 5 for 175 KIAS, a fly-by waypoint and a 60-degree course change, the RAD is .56 NM. Therefore, the minimum turn distance for the course transition at the IWP is  $1.93 - .56 = 1.37$  NM. The minimum turn distance for the second course transition at the FAWP is determined in a similar manner. From table 2 for 175 KIAS and a 30-degree course change, the minimum turn distance is 1.37 NM. From table 5 for 175 KIAS, a fly-by waypoint and a 30-degree course change, the RAD is .37 NM. Therefore, the minimum turn distance for the second transition at the FAWP is  $1.37 - .37 = 1.0$  NM. The minimum intermediate segment length is then  $1.37 + 1.0 = 2.37$  NM.

**Final Segment (FAWP - MAWP).** From table 6 with a course change of 30 degrees at the FAWP, the minimum final segment length is 3.5 degrees NM.

**c. Waypoint Definition.** When segments are aligned on a straight continuous course with no turns between approach segments prior to the MAWP, construct all preceding WP's using the MAWP as the reference WP. When segments are not aligned on a straight course, use the MAWP as the reference WP to construct the FAWP; use the FAWP to construct preceding WP if preceding segments are on a straight course; or use the IWP as the reference WP to construct the IAWP when there is a turn at the IWP.

**d. Course Change at Waypoints.** The departure course at a WP is the bearing from that WP to the following WP. The arrival course at the WP is the reciprocal of the course from that WP to the preceding WP, and the difference between the departure course and the arrival course at the WP equals the amount of turn at that WP.

**e. Minimum Safe Altitude.** A minimum safe altitude shall be established using the MAWP as the reference center. Develop sectors in accordance with TERPS, paragraph 221.

**7. IDENTIFICATION OF FMS INSTRUMENT APPROACH PROCEDURES (IAP).** IAP's, based on FMS, are identified by the prefix "FMS RNAV," followed by the runway number/letter, as appropriate; i.e., FMS RNAV RWY 17, FMS RNAV-A. In the case of a FMS transition to an ILS final segment, the IAP is identified as FMS/ILS to the appropriate runway. The IAP shall be annotated as follows: "FMS PROCEDURE - /G AIRCRAFT CERTIFICATION REQUIRED."

**8. HOLDING.** TERPS, chapter 2, section 9, applies, except paragraph 292d. When holding is at a FMS WP, the primary area of the selected pattern shall be large enough to contain the entire waypoint displacement area. To establish the area, refer to FAA Order 7130.3, Holding Pattern Criteria. Use 15 NM distance for terminal holding procedures and 30 NM distance for en route holding. Obtain leg-length information from Order 7130.3, appendix 1, holding course toward the NAVAID. Outbound-end reduction is not authorized.

## **SECTION 2. FMS NONPRECISION APPROACH CRITERIA**

**9. EN ROUTE AND FEEDER ROUTE CRITERIA.** Use en route waypoint displacement tolerances for en route waypoints. Use terminal waypoint displacement tolerances for en route waypoints used as feeder waypoints. For all other purposes, use en route criteria for both en route and feeder route construction. En route obstacle clearance areas are identified as primary and secondary. These designations apply to straight and turning segment obstacle clearance areas. The required angle of turn connecting en route segments to other en route, feeder or initial approach segments shall not exceed 120 degrees. Where the turn exceeds 15 degrees, expanded turning area construction methods as discussed below apply.

### **a. Primary Area.**

(1) **Width.** TERPS, chapter 15, paragraphs 1510a(2) and 1510a(3) apply.

(2) **Length.** The minimum length of an en route segment is determined as described in paragraph 6b(3). There is no maximum length for an en route segment. The fix displacement areas of consecutive waypoints shall not overlap.

### **b. Secondary Area.** TERPS, chapter 15, paragraphs 1510b(2) and 1510b(3) apply.

**c. Construction of Expanded Turning Areas.** Obstacle clearance areas shall be expanded to accommodate turns of more than 15 degrees. For fly-by waypoints inside turn expansion is constructed to accommodate turn anticipation. For fly-over waypoints outside turn expansion is applied to protect for the fly-over maneuver.

(1) **Fly-by Waypoint.** TERPS, chapter 15, paragraph 1510c(2) applies.

(2) **Fly-over Waypoint.** With reference to figure 3, determine the expanded area at the outside of the turn as follows:

(a) Using the applicable speed (250 KIAS at and below 10,000' MSL, 310 KIAS above 10,000' MSL) and turn angle, determine the RAD from table 5. Construct a line (ABCD in figure 3) perpendicular to the preceding route centerline the required RAD past the latest point the waypoint can be determined. This line is a base line for constructing arc boundaries.

(b) Using the applicable speed and turn angle, enter table 3 and determine the radius of turn. From a point (C in figure 3) on the arc base line, strike an outer primary area boundary arc of table 3 radius in the direction of turn beginning at the point (A in figure 3) where an extension of the outer line of the fix displacement area intersects the base line. Strike another arc of the same radius in the direction of turn

beginning at the point (B in figure 3) where an extension of the inner line of the fix displacement area intersects the base line. Connect the two outer primary area boundary arcs with a tangent line.

(c) From table 3 determine the minimum turn distance. From the plotted position of the waypoint, measure along the outbound course centerline the minimum turn distance (E in figure 3). Transfer this point along a line perpendicular to the courseline to the outer primary area boundary (F in figure 3). Connect a line from this point tangent to the outermost primary area boundary arc.

(d) From a point (G in figure 3) on the outer primary area boundary perpendicular to the inbound course at the plotted position of the fix, connect a tangent line to the first outer primary area boundary arc.

(e) Establish outer secondary area boundary arcs by striking arcs of table 3 radius plus 2 NM from the center points (C and D in figure 3) used for the primary area expansion. Connect the two outer secondary area boundary arcs with a tangent line.

(f) At the minimum turn distance determined in (c) above, transfer the turn completion point (E in figure 3) along a line perpendicular to the courseline to the outer secondary area boundary (H in figure 3). Connect a tangent line from this point to the outermost secondary area boundary arc.

(g) From a point on the outer secondary area boundary perpendicular to the inbound course at the plotted position of the fix (I in figure 3), connect a tangent line to the first outer secondary area boundary arc.

**d. Obstacle Clearance.** TERPS, paragraph 1511, applies.

## **10. APPROACH CRITERIA.**

**a. Approach Turning Area Expansion.** Obstacle clearance areas will be expanded to accommodate turns of more than 15 degrees at the IAWP, IWP and FAWP. See figures 4, 5, and 6. Outside turn expansion is not required at these waypoints. MAWP turn expansion criteria is contained in section 5 of this order. Construct the approach turning area expansion as follows:

(1) Determine the ATRK displacement tolerance from table 1. Measure this distance from the WP on the inbound course and plot a line perpendicular to the centerline.

(2) Locate a point on the edge of the primary area on the inside of the turn at the distance of turn anticipation (DTA) prior to the ATRK displacement line. The DTA is measured parallel to the course leading to the WP and is determined by the following formulas:

For turns greater than 15° and less than or equal to 90°  

$$DTA = 2 \times \tan(\text{turn angle} \div 2)$$

For turns greater than 90° and less than or equal to 105°  

$$DTA = 2.5 \times \tan(\text{turn angle} \div 2)$$

For turns greater than 105° and less than or equal to 120°  

$$DTA = 3 \times \tan(\text{turn angle} \div 2)$$

(3) From this point, splay the primary area by an angle equal to half the course change until this line intersects the primary area of a succeeding segment. Depending on procedure geometry, this may not be the primary area of the immediately following segment.

(4) Construct the secondary area boundary parallel with the expanded turn anticipation primary area boundary a distance of 1 NM. Extend the secondary area boundary line until it intersects another secondary segment area. Depending on procedure geometry, this may not be the secondary area of the immediately following segment.

(5) In the case of small turn angles, the primary or secondary turn expansion lines may not intersect another primary or secondary area boundary. In this case join the expanded areas at respective points abeam the succeeding WP.

(6) Evaluate primary and secondary areas using the ROC of the segment(s) following the turn WP. These general guidelines apply:

(a) Working from the primary area turn expansion line back toward the inside of the turn, connect all points which outline secondary area. This area will become primary area for obstacle evaluation purposes. If more than one segment's secondary area is outlined, divide the area for ROC application at the earliest point the second WP can be determined.

(b) To evaluate the secondary turn expansion area, connect the ends of the secondary turn expansion line to the ends of the primary turn expansion line. The area so enclosed will be evaluated as secondary area of the adjacent reevaluated primary segment. ROC for obstacles within this area is evaluated perpendicular to the primary area turn expansion line.

**b. Initial Approach Segment.** The initial approach segment begins at the IAWP and ends at the IWP. See figure 4.

**(1) Segmented Path.** A segmented initial approach segment is defined by multiple straight-line legs that begin and end with defined fly-by waypoints. See figure 6. If any of these waypoints are also defined as an IAWP, then paragraph 10b(4) applies and a separate evaluation for the newly defined initial segment is required, including all segment legs. The initial approach segment may contain up to four legs. Waypoints shall be located where the course changes and shall be named. Minimum leg lengths are determined as described in paragraph 6b(3) using the 220 KIAS column in table 2. Turning area expansion as described in paragraph 10a shall be applied to segmented path waypoints. Evaluate the primary and secondary turn expansion areas for the segment or leg following the turn waypoint. See figure 6.

**(2) Alignment.** The angle of intercept between initial legs and between an initial leg and the intermediate segment shall not exceed 120 degrees.

**(3) Length.** The initial approach segment has no standard length. It will be sufficient to permit any altitude changes required by the procedure. Total length of the initial segment including all legs of a segmented path shall not exceed 50 miles. Minimum individual segment length is determined as described in paragraph 6b(3).



(4) **Width.** The width of the initial segment shall remain at en route width until the latest position of the IAWP. The primary area tapers 90 degrees abeam this point inward at 30 degrees relative to centerline until reaching a width of 1 NM. The secondary area tapers to a width of 1 NM. The taper begins at the latest position of the IAWP abeam the point of taper of the primary area and tapers to a point abeam the primary area where it reaches its reduced width.

(5) **Obstacle Clearance.** Refer to TERPS, paragraph 232c.

(6) **Descent Gradient.** Refer to TERPS, paragraphs 232d and 288a.

c. **Intermediate Approach Segment.** The intermediate segment begins at the IWP and ends at the FAWP.

(1) **Alignment.** The course selected in the intermediate segment should be aligned with the final approach course. When this is not practical, the course change at the FAWP shall not exceed 30 degrees. Paragraph 10a applies for turning area expansion.

(2) **Length.** The minimum intermediate segment length is determined as described in paragraph 6b(3). The maximum intermediate length is 15 NM.

(3) **Width.**

(a) Primary area is 1 NM each side of centerline.

(b) Secondary area is 1 NM on each side of the primary area.

(4) **Obstacle Clearance.** TERPS, paragraph 242c, applies.

(5) **Descent Gradient.** TERPS, paragraph 242d, applies.

d. **Final Approach Segment.** The final approach segment begins at the FAWP and ends at the MAWP.

(1) **Alignment.**

(a) **Straight-In.** For a straight-in approach, the final approach course (FAC) shall not exceed 15 degrees from the runway centerline (RCL) extended. Optimum FAC is coincident with the RCL. Where the FAC is within 3 degrees of the RCL, the optimum alignment is to the runway threshold. Where the FAC exceeds 3 degrees from the RCL, the optimum alignment is to a point 3,000 feet from runway threshold on the RCL. Where operationally required, optional alignment is authorized to a point between and including the runway threshold and a point 3,000 feet prior to the runway threshold on the RCL, provided alignment is within 15 degrees of the RCL.

1 Except where the alignment is to the runway threshold, the mandatory location of the MAWP is at the intersection of the FAC and the RCL.

2 Where the alignment is to the runway threshold, the optimum location of the MAWP is at the threshold, with optional location of the MAWP anywhere along the FAC between the threshold and the FAWP.

**(b) Circling Alignment.** The optimum FAC alignment is to the center of the landing area, but may be to any portion of the usable landing surface. The optional location of the MAWP is anywhere along the FAC between the FAWP and the point abeam the nearest landing surface.

**(2) Area.** The area (straight and circling) considered for obstacle clearance starts at the earliest point of the FAWP displacement area and ends at the latest point of the MAWP displacement area or the runway threshold or a point abeam the runway threshold whichever is encountered last. See figure 7. The area extended to the threshold beyond the MAWP, when required, has a constant width for both primary and secondary areas and those dimensions equal the lateral dimensions at the MAWP. See figure 8.

**(3) Length.** The length of the final approach segment is measured from the plotted position of the FAWP to the runway threshold or a point abeam the threshold, whichever is encountered last. The optimum length is 5 NM. The maximum length is 10 NM. The minimum length shall provide adequate distance for an aircraft to meet the required descent and to regain course alignment when a turn is required over the FAWP. Table 6 is used to determine the minimum length of the final approach segment.

**(4) Width.**

(a) The final approach primary area is centered on the final approach course. It is 1 NM wide on each side of the course at the earliest point of the FAWP displacement area. This width remains constant until the latest point of the FAWP displacement area. It then tapers to the width of the XTRK displacement tolerance (0.6 NM on each side of the final approach course) at the latest point of the MAWP displacement.

(b) A secondary area is 1 NM wide is established on each side of the primary area.

**(5) Obstacle Clearance.**

**(a) Straight-In.** The minimum required obstruction clearance (ROC) in the primary area is 250 feet. In the secondary area, 250 feet of ROC shall be provided at the inner edge, tapering uniformly to zero feet at the outer edge.

**(b) Circling.** A minimum of 300 feet of ROC shall be provided in the circling approach area. TERPS, paragraph 260, applies.

**(6) Descent Gradient.** The optimum descent gradient is 300 feet per mile. Where a higher gradient is necessary, the maximum permissible descent gradient is 400 feet per mile.

**(7) Vertical Navigation (VNAV) Descent Angle.** Whenever possible, a final approach VNAV descent angle meeting the criteria in TERPS, paragraph 1523f, shall be published.

**e. Obstacle Rich Environment (ORE).** Due to the high degree of reliance on the FMS for navigation, redundant airborne equipment, surveillance, or special procedures may be required for certain procedures.

When a procedure is considered to be in an ORE, the procedure should be processed as a special, or a waiver must be issued by the FAA Flight Standards Service, Washington, D.C.

**(1) Assessment.** Whenever the minimum procedural altitude in an FMS approach procedure containing turns falls below the height of an obstacle located within 6 NM of the course centerline, an ORE assessment shall be made. For each such obstacle there is a "critical point." The critical point is that point on the outer edge of the secondary area having the shortest distance to the obstacle using a 15-degree splay from course centerline. The ORE assessment consists of determining whether a 40:1 incline starting from the critical point at the minimum procedural altitude clears the obstacle. Obstacles whose critical point is abeam or after the FAWP or obstacles whose critical point is abeam or prior to the IAWP do not require an ORE assessment.

**(2) Method.**

(a) Identify each obstacle higher than the minimum procedural altitude and located within 6 NM of the course centerline that requires an ORE assessment.

(b) Locate the critical point for each obstacle identified above. Because the outer edge of the secondary area might not be parallel to the course centerline, the line from the critical point to the obstacle might not be 15 degrees from the edge of the secondary area. However, the line from the critical point to the obstacle is always 105 degrees from a line perpendicular to the course centerline. Consequently, the critical point is located by sliding a 105-degree template along the outer edge of the secondary area (with its origin, or corner, on the outer edge of the area) until the 105-degree line touches the closest point of the obstacle. See figure 9.

(c) Determine whether a 40:1 incline starting from the critical point at the minimum procedural altitude clears the obstacle. This is done by measuring the distance in feet between the critical point and the obstacle and dividing that distance by 40. The quotient is added to the elevation of the critical point (i.e., the MINIMUM procedural altitude abeam the critical point) to compute the height of the 40:1 incline at the obstacle. If the elevation of the obstacle is higher than the height of the 40:1 incline, the environment is obstacle rich. A single penetration of the 40:1 incline is sufficient to make the approach environment obstacle rich. See figure 9.

(d) Obstacles A through D in figure 9 are evaluated to determine whether they require an ORE assessment:

A. This obstacle is below the minimum procedural altitude at its critical point (2,000 feet) and does not require an ORE assessment.

B. This obstacle is more than 6 NM from initial segment centerline and does not require an ORE assessment.

C. The 2,379-foot obstacle requires an ORE assessment because it is higher than the minimum procedural altitude abeam its critical point (2,000 feet). The 40:1 incline starts at this same altitude, 2,000 feet, at the critical point. The distance between the critical point and the obstacle is 14,000 feet.  $14,000' \div 40 = 350' + 2000' = 2350'$  which is 29 feet below the top of the obstacle. The environment is obstacle rich.

D. Although this obstacle is abeam the final approach segment, its critical point is abeam the intermediate segment. In addition, its 1,899-foot height is above the minimum procedural altitude of 1,500 feet. Consequently, it requires an ORE assessment. The 40:1 incline starts at 1,500 feet at the critical point. The distance between the critical point and the obstacle is 15,000 feet.  $15,000' \div 40 = 375' + 1500' = 1875'$  which is 24 feet below the top of the obstacle. The environment is obstacle rich.

### SECTION 3. FMS TRANSITION TO ILS FINAL APPROACH SEGMENT

**11. EN ROUTE AND FEEDER ROUTE CRITERIA.** Paragraph 9 applies.

**12. APPROACH CRITERIA.** See figure 10.

**a. Approach Turning Area Expansion.** Paragraph 10a applies.

**b. Initial Approach Segment.** Paragraph 10b applies, with the following exceptions:

(1) **Alignment.** The maximum angle of intercept between an initial segment and intermediate is 90 degrees.

(2) **Width.** The width of the initial segment shall remain at en route width until the latest position of the IAWP. The primary area tapers from 90 degrees abeam this point inward at 30 degrees relative to centerline until reaching a width of 1 NM or the maximum half-width of the ILS final approach area, whichever is greater. The ILS final approach area half-width is defined in TERPS, paragraph 930, and Order 8260.36, paragraph 16, and is found by using the formula  $500' + .15(F - 200')$ , where F is the distance from the threshold to the glideslope intercept point. The secondary area tapers to a width of 1 NM, beginning abeam the point of taper of the primary area and ending at a point abeam the primary area, where it reaches its reduced width.

**c. Intermediate Approach Segment.** The intermediate segment begins at the IWP and ends at the ILS glideslope intercept point (GSIP).

(1) **Alignment.** The intermediate segment course shall be an extension of the final approach course.

(2) **Length.** The minimum length of the intermediate segment depends on the angle of turn at the IWP. Table 7 specifies minimum intermediate segment lengths.

(3) **Width.** See figure 11. The primary intermediate segment half-width is 1 NM at the earliest point of the IWP displacement area. This width remains constant until the latest point of the IWP displacement area. It then tapers to the half width of the ILS final approach area at the GSIP. In the case where the maximum half width of the ILS final approach area exceeds 1 NM, then the primary intermediate width is constant at the maximum half-width of the ILS final approach area. The width of the secondary intermediate segment is 1 NM each side of the primary area at the earliest point of the IWP displacement area. This width remains constant until the latest point of the IWP displacement area. It then tapers to the width of the ILS secondary area at the GSIP.

(4) **Obstacle Clearance.** TERPS, paragraph 242c, applies.

(5) **Descent Gradient.** TERPS, paragraphs 242d and 923, apply.

(6) **Altitude Selection.** The intermediate segment altitude shall not be less than the glideslope intercept altitude.

(7) **IWP Placement.** In order to assure localizer course capture, the IWP shall be laterally located in the center of the localizer course and shall be placed no closer to the runway threshold than explained in this paragraph. For approaches where there is a course change of less than 15 degrees at the IWP, the IWP shall be no closer to the threshold than a point where the localizer course half-width is 0.3 NM. For approaches with course changes at the IWP of more than 15 degrees, additional distance to account for turn anticipation shall be added to determine minimum IWP distance from the runway threshold. The minimum IWP distance from runway threshold is determined as follows:

(a) Compute the distance from the runway threshold to the point where the localizer course half-width is 0.3 NM.

$$D_1 = D * \left[ \frac{.3}{(1/2 \text{ W at Thld})} - .000164578 \right]$$

Where:

D = runway threshold to localizer antenna distance in feet.

(1/2 W at Thld) = half-width of localizer at runway threshold in feet.

D<sub>1</sub> = distance in NM from runway threshold to point where localizer course half-width is 0.3 NM.

Where there is a course change of 15 degrees or less at the IWP, D<sub>1</sub> is also the minimum IWP distance from the runway threshold.

**Example 1.** See figure 12. Given a runway length of 10,000 feet, a localizer antenna to runway end distance of 1,000 feet, a localizer course width of ± 350' at the runway threshold and no turn at the IWP, compute the minimum IWP distance.

$$D = 10,000' + 1,000' = 11,000'$$

$$D_1 = 11,000' * \left( \frac{.3}{350'} - .000164578 \right) = 7.62 \text{ NM}$$

Minimum IWP distance is 7.62 NM.

(b) For turns of more than 15 degrees at the IWP, additional distance must be added to D<sub>1</sub> to account for the turn. This additional distance, D<sub>2</sub>, is found by entering table 2 with the IWP course change and reading the minimum turn distance from the 175 KIAS column. D<sub>2</sub> is added to D<sub>1</sub> to find the minimum IWP distance.

**Example 2.** See figure 13. The runway length is 7,000 feet, the localizer course width is tailored  $\pm 350'$  at the threshold and the localizer is located 1,000 feet from the end of the runway. The initial and intermediate segments differ by 30 degrees. Compute the minimum IWP distance.

$$D = 7,000' + 1,000' = 8,000'$$

$$D_1 = 8,000' * \left( \frac{.3}{350'} - .000164578 \right) = 5.54 \text{ NM}$$

$$D_2 = 1.37 \text{ NM (from table 2, 175 KIAS column, turn angle of } 30^\circ)$$

$$\text{Minimum IWP distance} = D_1 + D_2 = 5.54 + 1.37 = 6.91 \text{ NM.}$$

**Example 3.** See figure 14. The runway length is 10,000 feet, the localizer course width is tailored  $\pm 350'$  at the threshold and the localizer is located 1,000 feet from the end of the runway. The initial and intermediate segments differ by 90 degrees. Compute the minimum IWP distance.

$$D = 10,000' + 1,000' = 11,000'$$

$$D_1 = 11,000' * \left( \frac{.3}{350'} - .000164578 \right) = 7.62 \text{ NM}$$

$$D_2 = 2.93 \text{ NM (from table 2, 175 KIAS column, turn angle of } 90^\circ)$$

$$\text{Minimum IWP distance} = D_1 + D_2 = 7.62 + 2.93 = 10.55 \text{ NM.}$$

**d. ILS Final Approach Segment.** TERPS, chapter 9, section 3, or for new ILS installations Order 8260.36, paragraph 16, applies. See figure 11.

**e. Obstacle Rich Environment.** Paragraph 10e applies.

## SECTION 4. FMS DEPARTURE CRITERIA

### 13. FMS DEPARTURE CRITERIA.

**a. Route.** The departure route begins at the TOWP and consists of a sequence of connected straight flight segments. Except in the case of a displaced threshold, the TOWP shall be the RWP. If the threshold is displaced, use the start of the usable runway for the TOWP. A fly-by or fly-over waypoint shall be specified at the beginning and end of each segment. The waypoint at which the route ends shall not be located prior to the point where the aircraft, climbing at the minimum prescribed climb gradient for each segment, reaches the minimum altitude for en route flight. FMS departure and en route flight segments shall be contiguous; i.e., the last waypoint of an FMS departure procedure shall be an en route fix.

(1) The first segment in the procedure begins at the TOWP and ends at a waypoint on the extended runway centerline that should be at least 2 NM beyond the departure end of the runway (DER). In addition, if the first segment terminates at a fly-by waypoint, the minimum turn distance from table 2 must be added.

If the first waypoint is less than 2 NM beyond the DER, a climb gradient calculation shall be made using the following formula:

$$G = \frac{400}{D}$$

Where: G = climb gradient (ft/NM).

D = distance from DER measured along the route centerline (NM).

**Example:** The first waypoint is located 1.0 NM beyond the DER. The required climb gradient is:

$$G = \frac{400}{1.0} = 400 \text{ ft} / \text{NM}$$

(2) The minimum segment length for any segment after the first is the greater of 0.6 NM or the minimum turn distance from either table 2 (for segments starting at a fly-by waypoint) or table 3 (for segments starting at a fly-over waypoint). In addition, for segments terminating at a fly-by waypoint, the applicable minimum turn distance from table 2 must be added at the end of the segment. See figures 1A, 1B, 1C, 1D and 1E.

(3) The angle of intersection between adjacent segments shall not exceed 120 degrees.

#### **b. Departure Area.**

**(1) Primary Area.** The primary area has a width of 1,000 feet ( $\pm 500$  feet from centerline) at the DER and splays at an angle of 7.5 degrees relative to runway centerline to a width of  $\pm 0.6$  NM (XTRK fix displacement tolerance). (See figure 16.) The primary area shall be expanded for turns. The size of the turn expansion area increases with speed. Use 250 KIAS to determine turn radii and distances from tables 2, 3, and 8 when the route ends before the aircraft reaches 10,000 feet MSL and 310 KIAS when the route includes flight above 10,000 feet MSL. If operational advantage can be obtained by using smaller turn radii and distances, restrict airspeed to 160 KIAS, 175 KIAS, 220 KIAS, or 250 KIAS and annotate the procedure, accordingly. Departure area construction at turn waypoints depends on whether the primary area 7.5-degree splay reaches a width of  $\pm 0.6$  NM prior to the waypoint.

**(a) Fly-by Waypoints (7.5-Degree Splay Incomplete).** In this case, the primary area width has not reached  $\pm 0.6$  NM prior to reaching the waypoint. Construct the outer edge of the primary area as follows: Transfer the width of the splay abeam the waypoint via an arc to the following segment. The arc is of radius equal to the attained half-width of the preceding segment (CB in figure 17) and is centered at the waypoint. Extend the arc to a line perpendicular to the centerline of the following segment and passing through the waypoint (A'E' in figure 17). Continue the 7.5-degree splay from that point to a width of  $\pm 0.6$  NM (B'F in figure 17). Construct the primary area inside fillet as follows: First, mirror the outer edge of the primary area beyond the waypoint (B'F in figure 17) across the centerline of the segment following the waypoint (D'G in figure 17). For turn angles 10 degrees through 120 degrees, fillet the inside of the primary area using the inside turn expansion radius from table 2 for the maximum selected airspeed. The center of the fillet is constructed on the bisector of the angle formed by edges of the primary area on the inside of the turn;

i.e., angle JHI is equal to angle IHG in figure 17. For turn angles less than 10 degrees, no fillet is required on the inside of the turn.

**(b) Fly-by Waypoints (7.5-Degree Splay Complete).** For turn angles 10 degrees through 120 degrees, fillet the outside of the primary area using the outside turn reduction radius from table 8. Fillet the inside of the primary area using the inside turn expansion radius from table 2 for the maximum selected airspeed. The center of this fillet is constructed on the bisector of the angle formed by the edges of the primary area on the inside of the turn; i.e., angle ABC is equal to angle CBD in figure 18. See figure 18. For turn angles less than 10 degrees, extend the primary area boundaries until they intersect. See figure 19.

**(c) Fly-over Waypoints (7.5-Degree Splay Incomplete).** In this case, the primary area width has not reached  $\pm 0.6$  NM prior to reaching the waypoint. For turn angles less than 10 degrees, extend the primary area boundaries until they intersect. See figure 19. For turn angles 10 degrees or greater, construct the outer edge of the primary area as follows: First, extend the primary area beyond the fly-over waypoint by 0.3 NM (ATRK fix displacement tolerance) plus the roll anticipation distance from table 5 (F and G in figure 20). The width of this extension shall not exceed  $\pm 0.6$  NM. Next, construct the outside turn expansion by drawing an arc tangent to the outside extended primary area (F in figure 20). The center of this arc (A in figure 20) is located on a line connecting the endpoints of the extended primary area; i.e., an extension of line FG in figure 20. Determine the radius from table 3 for the maximum selected airspeed. Using this same radius, draw a second arc tangent to the inside extended primary area (G in figure 20). The center of this arc (A' in figure 20) is also located on the line connecting the endpoints of the extended primary area; i.e., the same line as A in figure 20. Connect the two arcs by drawing a line (BB' in figure 20) tangent to the two arcs. Next, construct a line (DD' in figure 20) perpendicular to the centerline of the segment following the fly-over waypoint. Position this line at a distance from the fly-over waypoint specified in the minimum turn distance column of table 3 for the maximum selected airspeed. Points D and D' are located 0.6 NM on either side of the segment centerline, respectively. Draw a line (D'E in figure 20) from the intersection of this perpendicular and the outside primary area boundary tangent to the outermost turn expansion arc. Construct the inner edge of the primary area as follows: Transfer the width of the splay abeam the waypoint via an arc to the following segment. The arc is of radius equal to the attained half-width of the preceding segment (HI in figure 20) and is centered at the waypoint. Extend the arc to a line perpendicular to the centerline of the following segments and passing through the waypoint (KH in figure 20). Continue the 7.5-degree splay from that point to a width of  $\pm 0.6$  NM.

**(d) Fly-over Waypoints (7.5-Degree Splay Complete).** In this case, the primary area width has reached  $\pm 0.6$  NM prior to reaching the waypoint. For turn angles less than 10 degrees, extend the primary area boundaries until they intersect. See figure 19. For turn angles 10 degrees or greater, construct the outer edge of the primary area as follows: First, extend the primary area beyond the fly-over waypoint by 0.3 NM (ATRK fix displacement tolerance) plus the roll anticipation distance from table 5 (F and G in figure 21). Next, construct the outside turn expansion by drawing an arc tangent to the outside extended primary area (F in figure 21). The center of this arc (A in figure 21) is located on a line connecting the endpoints of the extended primary area; i.e., an extension of line FG in figure 21. Determine the radius from table 3 for the maximum selected airspeed. Using this same radius, draw a second arc tangent to the inside extended primary area (G in figure 21). The center of this arc (A' in figure 21) is also located on the line connecting the endpoints of the extended primary area; i.e., the same line as A in figure 21. Connect the two arcs by drawing a line (BB' in figure 21) tangent to the two arcs. Next, construct a line (DD' in figure 21) perpendicular to the centerline of the segment following the fly-over waypoint. Position this line at a distance from the fly-over waypoint specified in the minimum turn distance column of table 3 for the maximum



selected airspeed. Points D and D' are located 0.6 NM on either side of the segment centerline, respectively. Draw a line (D'E in figure 21) from the intersection of this perpendicular and the outside primary area boundary tangent to the outermost turn expansion arc.

**(2) Secondary Area.** The secondary area is constructed on both sides of the primary area. It begins at the DER and splays at an angle of 7.5 degrees measured from the edge of the primary area. After the splay reaches a width of 1 NM, measured perpendicular to the edge of the primary area, the secondary area width remains 1 NM. See figure 16. Secondary area construction at turn waypoints depends on whether the secondary area 7.5-degree splay reaches a width of  $\pm 1.0$  NM prior to the waypoint.

**(a) Fly-by Waypoints (7.5-Degree Splay Incomplete).** In this case, the secondary area width has not reached  $\pm 1.0$  NM prior to reaching the waypoint. Construct the outer edge of the secondary area as follows: Transfer the width of the splay abeam the waypoint via an arc to the following segment. The arc is of radius equal to the attained half-width of the preceding segment (CA in figure 17) and is centered at the waypoint. Extend the arc to a line perpendicular to the centerline of the following segment and passing through the waypoint (A'E' in figure 17). Continue the 7.5-degree splay from that point to a width of  $\pm 1.0$  NM (A'KL in figure 17). Construct the secondary area inside fillet as follows: First, mirror the outer edge of the secondary area beyond the waypoint (A'K in figure 17) across the centerline of the segment following the waypoint (E'M in figure 17). For turn angles 10 degrees through 120 degrees, fillet the inside of the secondary area using the inside turn expansion radius from table 2 for the maximum selected airspeed. The center of the fillet is constructed on the bisector of the angle formed by edges of the secondary area on the inside of the turn; i.e., angle JE'O is equal to angle OE'M in figure 17. For turn angles less than 10 degrees, no fillet is required on the inside of the turn.

**(b) Fly-by Waypoints (7.5-Degree Splay Complete).** For turn angles 10 degrees through 120 degrees, fillet the outside of the secondary area using the outside turn reduction radius from table 8. Fillet the inside of the secondary area using the inside turn expansion radius from table 2 for the maximum selected airspeed minus 1 NM. The center of this fillet is constructed on the bisector of the angle formed by the edges of the secondary area on the inside of the turn. See figure 18. For turn angles less than 10 degrees, extend the secondary area boundaries until they intersect. See figure 19.

**(c) Fly-over Waypoints (7.5-Degree Splay Incomplete).** In this case, the secondary area width has not reached 1.0 NM prior to reaching the waypoint. For turn angles less than 10 degrees, extend the secondary area boundaries until they intersect. See figure 19. For turn angles 10 degrees or greater, construct the outer edge of the secondary area as follows: The secondary area begins at the edge of the primary area at the DER and splays 7.5 degrees from the edge of the primary area. Extend the edge of the secondary area until it joins an arc concentric with the primary area turn expansion (M in figure 20). The concentric arc is constructed using the outside turn expansion radius determined from table 3 for the maximum selected airspeed plus 1 NM. The center of this arc is the same as for the primary outer turn expansion area (A in figure 20). Using this same radius, draw a second arc concentric with the other primary turn expansion arc; i.e., centered at A' in figure 20. Connect the two arcs by drawing a line (PP' in figure 20) tangent to the two arcs. The remainder of the secondary area has a width of 1 NM and is constructed parallel to the edge of the primary area (QR in figure 20). Construct the inner edge of the secondary area as follows: The secondary area begins at the edge of the primary area at the DER and splays 7.5 degrees from the edge of the primary area. Transfer the width of the splay abeam the waypoint via an arc to the following segment. The arc is of radius equal to the attained half-width of the preceding segment (HJ in figure 20) and is centered at the waypoint. Extend the arc to a line perpendicular to the centerline of the following segments

and passing through the waypoint (LH in figure 20). Continue the 7.5-degree splay from that point to a width of 1 NM measured perpendicular to the edge of the primary area.

**(d) Fly-over Waypoints (7.5-Degree Splay Complete).** In this case, the secondary area width has reached 1.0 NM prior to reaching the waypoint. For turn angles less than 10 degrees, extend the secondary area boundaries until they intersect. See figure 19. For turn angles 10 degrees or greater construct the outer edge of the secondary area as follows: Extend the edge of the secondary area until it joins an arc concentric with the primary area turn expansion. The concentric arc is constructed using the outside turn expansion radius determined from table 3 for the maximum selected airspeed plus 1 NM. The center of this arc is the same as for the primary outer turn expansion area (A in figure 21). Using this same radius, draw a second arc concentric with the other primary turn expansion arc; i.e., centered at A' in figure 21. Connect the two arcs by drawing a line (HH' in figure 21) tangent to the two arcs. The remainder of the secondary area has a width of 1 NM and is constructed parallel to the edge of the primary area (JK in figure 21). Construct the inner edge of the secondary area parallel to the edge of the primary area with a width of 1 NM.

**c. Obstacle Clearance.** The area considered for obstacle clearance for a flight segment between two waypoints starts at the earliest point the beginning waypoint can be identified and ends at the plotted position of the ending waypoint. Waypoint displacement tolerance for the TOWP need not be considered for departure procedures.

**(1) Primary Area.** In the primary area, an obstacle identification surface (OIS) of 40:1 is used. Obstacles which penetrate the OIS shall be avoided by specifying a climb gradient that will provide the required obstacle clearance (ROC).

(a) The Obstacle Identification Surface (OIS) (40:1) begins at the height of the DER and rises in the direction of departure. In turn expansion areas, the OIS rises along the shortest distance in the primary area to the obstacle; i.e., the 40:1 surface rises along the shortest possible flight path within the primary area.

(b) The minimum climb gradient required to clear an obstacle is determined from the formula:

$$G = \frac{48D + H}{D}$$

Where: G = Climb gradient (ft/NM).

H = Height of obstacle above DER (ft).

D = Distance from DER measured along the shortest distance within the primary area (NM).

(c) The climb gradient applied shall be the greatest of 200 ft/NM, the largest gradient required for obstacle clearance from the gradient required by paragraph 12a(1), paragraph 13c(1)(b), or that requested by the proponent. A climb gradient in excess of 500 feet/NM is approved on a case-by-case basis by the FAA Flight Standards Service, Washington, D.C.

1 Climb gradients begin at the DER.

2 Climb gradients shall be specified to a height at least 300 feet above the DER.

3 Climb gradients shall be specified (next higher 10-ft/NM increments) to an MSL altitude (next higher 100-foot increments) or waypoint where a gradient greater than 200 ft/NM is no longer required.

4 TERPS, paragraph 323a, applies.

(2) **Secondary Area.** The secondary area has a slope of 7:1, perpendicular to the edge of a turn expansion area. When there is no turn expansion area adjacent to the secondary area, the secondary area 7:1 slope is perpendicular to segment centerline. To evaluate an obstacle in the secondary area, determine the height of an equivalent obstacle on the edge of the primary area. Then, evaluate the equivalent obstacle height relative to the 40:1 OIS. The minimum climb gradient required to clear the obstacle is determined, as in paragraph 13c(1)(b), above, for the equivalent obstacle.

(3) **Climb Gradient Example.** Figure 22 shows a climb gradient computation example. The turn angle at the first waypoint is 30 degrees, and because of operational restrictions, 160 KIAS criteria from table 2 is used. A 9,839-foot MSL obstacle is located in the secondary area, 2,700 feet from the edge of the primary area, as shown in figure 22. The height of an equivalent obstacle on the edge of the primary area must first be determined:

$$7:1 \text{ slope to edge of primary area: } \frac{2,700'}{7} = 385.7'$$

$$\begin{array}{r} 9,839.0' \\ \text{Height of equivalent obstacle: } \quad \frac{-385.7'}{9,453.3'} \end{array}$$

Next, the distance (D) of the equivalent obstacle from the DER is determined:

$$D = \overline{AB} + \overline{BC} + \overline{CD} \text{ where A, B, C and D are shown in figure 22.}$$

The distance from A to B (denoted as  $\overline{AB}$ ) is measured as 7,364 feet. The distance around the arc from B to C (denoted as  $\overline{BC}$ ) can be computed as follows:

$$\overline{BC} = (\text{arc radius in feet}) \times (\text{angle of turn}) \times (.017453).$$

From table 2 for 160 KIAS and a turn angle of 30 degrees the radius is 3.28 NM or 19929.6 feet. Therefore,  $\overline{BC} = (19929.6') \times (30^\circ) \times (.017453) = 10,435'$ .

The distance from C to D (denoted as  $\overline{CD}$ ) is measured as 3545 feet. Then,

$$D = 7364' + 10,435' + 3545' = 21,344' = 3.51 \text{ NM.}$$

Next, the height of the OIS at the equivalent obstacle is determined:

$$40:1 \text{ slope from DER: } \frac{21,344'}{40} = 533.6'$$

$$\begin{array}{r} \text{Elev DER} \quad 7,640.0' \\ 40:1 \quad +533.6' \\ \text{OIS} \quad \hline 8,173.6' \end{array}$$

Because the height of the obstacle (9,453.3 feet) is greater than the height of the OIS (8,173.6 feet), an OIS penetration exists. The minimum climb gradient is now computed:

H = Height of equivalent obstacle above DER:

$$\begin{array}{r} \text{OBST} \quad 9,453.3' \\ \text{Elev DER} \quad -7,640.0' \\ \text{H} \quad \hline 1,813.3' \end{array}$$

$$G = \frac{48D + H}{D} = \frac{48(3.513) + 1813.3}{3.513} = 564.2'/\text{NM}$$

The required climb gradient is: MIN CLIMB OF 570' PER NM TO 9500. Since the climb gradient exceeds 500 feet/NM, approval from the FAA Flight Standards Service, Washington, D.C., is required.

## SECTION 5. FMS MISSED APPROACH CRITERIA

### 14. FMS MISSED APPROACH (MA) CRITERIA.

**a. General.** These criteria are applicable to FMS Nonprecision, Microwave Landing System (MLS), Instrument Landing System (ILS), and localizer approaches which satisfy the alignment criteria of this order, paragraph 10d; Order 8260.36, paragraph 16a; and TERPS, paragraphs 930a and 952, respectively.

**b. Route.** The FMS navigation routing begins at the RWP for precision approaches and at the MAWP for LOC or FMS nonprecision approaches. See figures 23, 24, 25, and 26. The route consists of a sequence of connected straight flight segments. A fly-by or fly-over waypoint shall be specified at the beginning and end of each segment. The waypoint at which the route ends shall not be located prior to the point where the aircraft, climbing at the minimum prescribed climb gradient for each segment, reaches the minimum altitude for en route flight or holding, whichever is appropriate. The missed approach route should be the same as the FMS departure route for the runway served.

(1) The minimum distance from the missed approach point to the end of the first segment is 1.5 NM, where the first segment ends at a fly-over waypoint. Where the first segment ends at a fly-by waypoint, the minimum distance from the missed approach point to the end of the first segment is 1.5 NM, plus the applicable minimum turn distance from table 2.

(2) The minimum segment length for any segment after the first is the greater of 0.6 NM or the minimum turn distance from table 2 (for segments starting at a fly-by waypoint) or table 3 (for segments starting at a fly-over waypoint). In addition, for segments terminating at a fly-by waypoint, the applicable minimum turn distance from table 2 at the end of the segment must be added. See figures 1A, 1B, 1C, 1D, and 1E.

(3) For FMS nonprecision missed approach, turns at the MAWP shall not exceed 3 degrees.

(4) The angle of intersection between adjacent segments shall not exceed 120 degrees.

### c. Missed Approach Area.

#### (1) Primary Area.

(a) **FMS Nonprecision Procedures.** The primary area begins at the earliest point the MAWP can be identified (0.3 NM prior to the waypoint). The width of the missed approach area at the point where the primary area begins is the same as the final approach segment primary area ( $\pm 0.6$  NM). See figure 23.

(b) **Localizer Procedures.** The primary area begins at the earliest point the missed approach waypoint can be identified (0.3 NM prior to the waypoint). The width of the missed approach area at the point where the primary area begins is the same as the final approach segment primary area width at that point. The missed approach area splays at 7.5 degrees to a width of 0.6 NM (XTRK fix displacement tolerance). See figure 24.

(c) **ILS and MLS Procedures.** The primary area begins at the missed approach point. The width of the missed approach primary area at the missed approach point is the same as the final approach segment primary area width at that point. The missed approach area splays at 7.5 degrees to a width of 0.6 NM. See figures 25 and 27.

(d) **Construction for Procedures Offset 3 Degrees or Less.** The missed approach primary area splays at 7.5 degrees relative to the offset course from a point (B in figures 26 and 28) located on the outside edge of the primary area at the missed approach point. The splay continues to a point (C in figures 26 and 28) located on a line perpendicular to the segment centerline through the RWP. Transfer the attained width (X in figures 26 and 28) to a point (D in figures 26 and 28) on the same perpendicular line extended to the opposite side of segment centerline. From the two points determined above (C and D in figures 26 and 28) continue the 7.5 degree splays relative to segment centerline to a width of  $\pm 0.6$  NM. See figures 26 and 28.

(e) **Turn Expansion Areas.** Paragraphs 13b(1)(a) through 13b(1)(d) apply to primary area turn expansion.

(2) **Secondary Area.** The secondary area is constructed on both sides of the primary area.

(a) **FMS Nonprecision Procedures.** The secondary area begins at the earliest point the MAWP can be identified (0.3 NM prior to the waypoint). The width of the secondary area is the same as the final approach segment secondary area (1 NM). See figure 23.

(b) **Localizer Procedures.** For localizer approaches, the secondary area begins at the earliest point the missed approach waypoint can be identified (0.3 NM prior to the waypoint). It has zero width at this point. The total segment width increases to  $\pm 0.5$  NM at a point 1.5 NM from the missed approach waypoint. Beyond this point, the secondary area splays at an angle of 15 degrees relative to segment centerline until reaching a width of 1 NM, measured perpendicular to the edge of the primary area. Thereafter, the secondary area width is 1 NM. See figure 24.

(c) **ILS and MLS Procedures.** For ILS procedures designed using TERPS, section 1 is constructed in accordance with paragraph 942a. Similarly, for ILS and MLS procedures designed using FAA Order 8260.36, section 1 is constructed in accordance with paragraph 19a. That portion of section 1 not contained in the primary area is secondary area. See figures 25 and 27. Beyond the end of section 1, the secondary area splays at an angle of 15 degrees relative to segment centerline until reaching a width of 1 NM, measured perpendicular to the primary boundary. Thereafter, the secondary area width is 1 NM.

(d) **Construction for Procedures Offset 3 Degrees or Less.** Construct section 1 only on the outside of the turn at the runway waypoint (BE in figures 26 and 28). Construct a line through the outside corner of section 1, perpendicular to the centerline of the segment following the runway waypoint (EF in figure 26). Transfer the width of this line (width "Y" in figures 26 and 28) to the inside of the turn (G in figures 26 and 28). Construct the inside edge of the primary area by drawing a line from the edge of the primary area abeam the missed approach point to this point (AG in figures 26 and 28). The secondary area then splays at an angle of 15 degrees relative to segment centerline, to a width of 1 NM, measured perpendicular from the edge of the primary area.

(e) **Turn Expansion Areas.** Paragraphs 13b(2)(a) through 13b(2)(d) apply to secondary area turn expansion.

#### **d. Obstacle Clearance.**

(1) **Primary Area.** The 40:1 missed approach surface for a FMS nonprecision approach begins at the edge of the MAWP displacement tolerance area (A-B in figure 23). The height of the missed approach surface at its beginning is determined by subtracting the required final approach obstacle clearance and any minima adjustments from the MDA. The 40:1 missed approach surface begins at the height specified in TERPS, paragraph 957, for localizer approaches. For ILS procedures designed using TERPS, the 40:1 missed approach surface begins at the height specified in paragraph 944a. For MLS procedures and ILS procedures designed using FAA Order 8260.36, paragraph 19d, applies, and the 40:1 missed approach surface begins at the end of section 1. Obstacles which penetrate the missed approach surface shall be avoided by increasing the MDA or DH or specifying a climb gradient that will provide the ROC.

- (a) The minimum climb gradient required to clear an obstacle is determined from the formula:

$$G = \frac{48D + H}{D}$$

Where G = Climb gradient (ft/NM)

H = Height of obstacle above start of the missed approach surface (ft)

D = Distance from the missed approach point for ILS and MLS procedures measured along the shortest distance within the primary area (NM). Distance from the latest point the missed approach point can be identified (0.3 NM beyond the missed approach point) for FMS nonprecision and localizer procedures.

- (b) The climb gradient applied shall be the greatest of 200 ft/NM, the largest gradient required for obstacle clearance from paragraph 13d(1)(a), above, or that requested by the proponent. Any procedure requiring a missed approach climb gradient in excess of 200 ft/NM shall be processed as a special procedure.

**(2) Secondary Area.** The secondary area has a slope of 7:1, perpendicular to the edge of the turn expansion area. When there is no turn expansion area adjacent to the secondary area, the secondary area 7:1 slope is perpendicular to segment centerline. To evaluate an obstacle in the secondary area, determine the height of an equivalent obstacle on the edge of the primary area. Then, evaluate the equivalent obstacle height relative to the 40:1 OIS.

**15. TAILORED PROCEDURES.** Procedure construction data contained in tables 2, 3, and 5 is derived from a mathematical model. Operational advantage may be obtained by tailoring the parameters of this model to the specific site, aircraft operating characteristics, and other operational limitations; e.g., wind restrictions. A computer program has been developed by the Standards Development Branch, AFS-421, to generate tailored data in lieu of tables 2, 3, and 5. Use of this program is approved on a case-by-case basis by the FAA Flight Standards Service, Washington, D.C.

**16. FMS APPROACH PROCEDURE SCREENING MODEL.** The approach criteria contained in this order is predicated on the FMS Navigational System Error (NSE) being no greater than 0.3 NM. For purposes of this order, FMS navigation system performance is based on a Kalman filter position solution using inputs from multiple Inertial Reference Units (IRU's) and single or multiple DME/DME pairs. Individual DME availability and geometry between DME/DME pairs can affect the NSE and can cause the NSE to exceed the required 0.3 NM. In order to assist the procedures specialist in determining whether the 0.3 NM NSE can be maintained throughout a particular approach, the Standards Development Branch, AFS-421, has developed a computer program which contains a simple Kalman filter model. The model uses statistical distributions for IRU and DME errors and has access to a database containing information on all DME locations within the United States. The specialist shall enter the route of flight for each proposed procedure, and the program will compute a theoretical NSE value each nautical mile along the flight path. If each of these model-generated NSE values is less than or equal to 0.3 NM, then, the proposed procedure is feasible. In addition, if the maintenance of 0.3 NM NSE is based on the availability of one or more individual DME facilities, the model will flag these as being "CRITICAL FACILITIES." (NOTE: The model described above is only a procedure development tool to test the initial feasibility of a proposed approach. A successful outcome for a particular approach is not a substitute for further testing in a suitably equipped simulator or aircraft. Similarly, an unsuccessful outcome is not the final arbiter of the feasibility of any particular approach. Additional investigation, which may include a test flight by either an FAA Flight

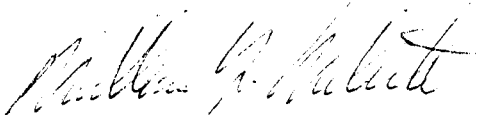
Inspection Area Office or the proponent, or a simulated flight in a suitably equipped simulator, shall be accomplished.)

**17. INFORMATION UPDATE.** Any deficiencies found, clarification needed, or improvements to be suggested regarding the content of this order, shall be forwarded for consideration to:

DOT/FAA  
ATTN: Flight Procedures Branch, AFS-440  
P.O. Box 25082  
Oklahoma City, OK 73125

**a. Your Assistance is Welcome.** FAA Form 1320-19, Directive Feedback Information, is included at the end of this order for your convenience.

**b. Use the "Other Comments" block of this form to provide a complete explanation of why the suggested change is necessary.**



William J. White  
Deputy Director, Flight Standards Service



**APPENDIX 1. FIGURES AND TABLES**

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Figure 1A. MINIMUM SEGMENT LENGTH  
FLY-OVER TO FLY-BY, Paragraph 6b(3).

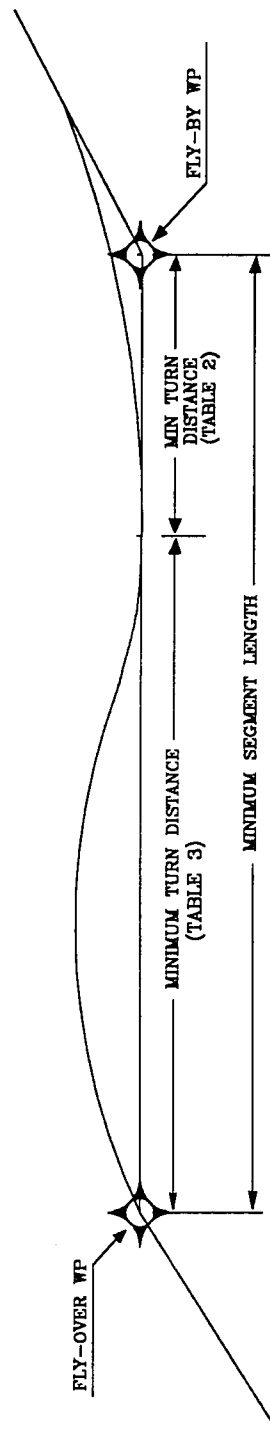


Figure 1B. MINIMUM SEGMENT LENGTH  
FLY-OVER TO FLY-OVER, Paragraph 6b(3).

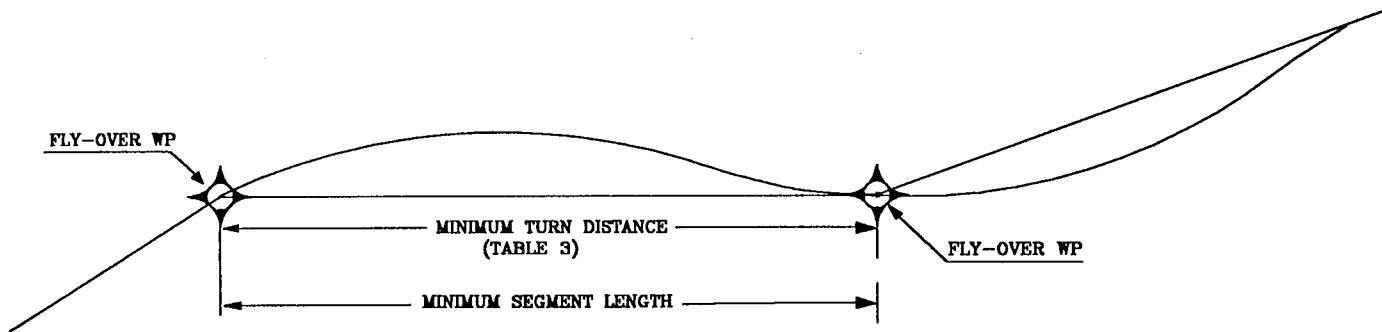


Figure 1C. MINIMUM SEGMENT LENGTH  
FLY-BY TO FLY-BY, Paragraph 6b(3).

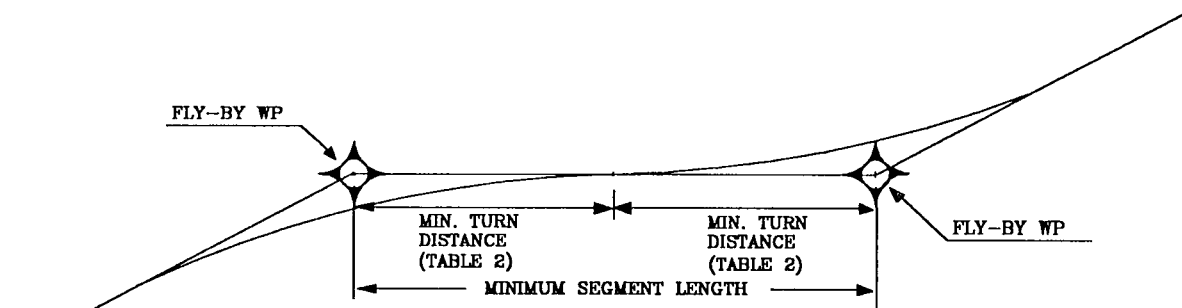


Figure 1D. MINIMUM SEGMENT LENGTH  
FLY-BY TO FLY-OVER, Paragraph 6b(3).

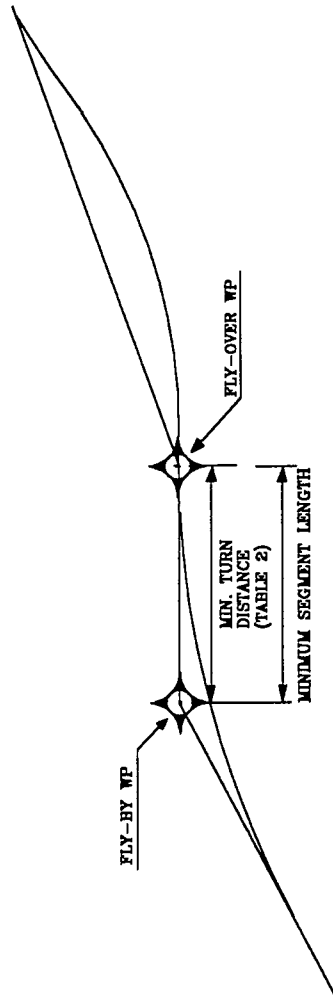


Figure 1E. MINIMUM SEGMENT LENGTH  
 FLY-BY TO FLY-BY (Turn in same direction),  
 Paragraph 6b(3).

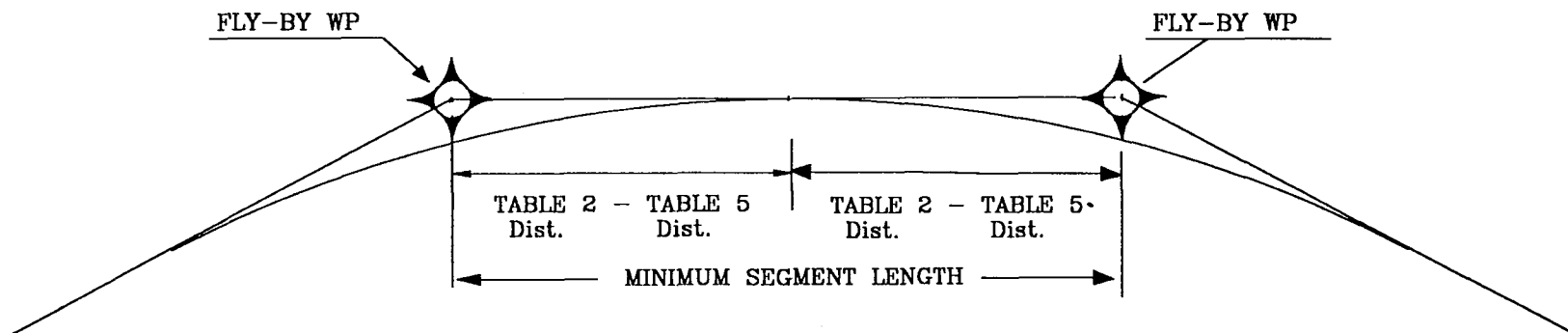


FIGURE 2. MINIMUM SEGMENT LENGTH DETERMINATION.  
Paragraph 6b(3)(e).

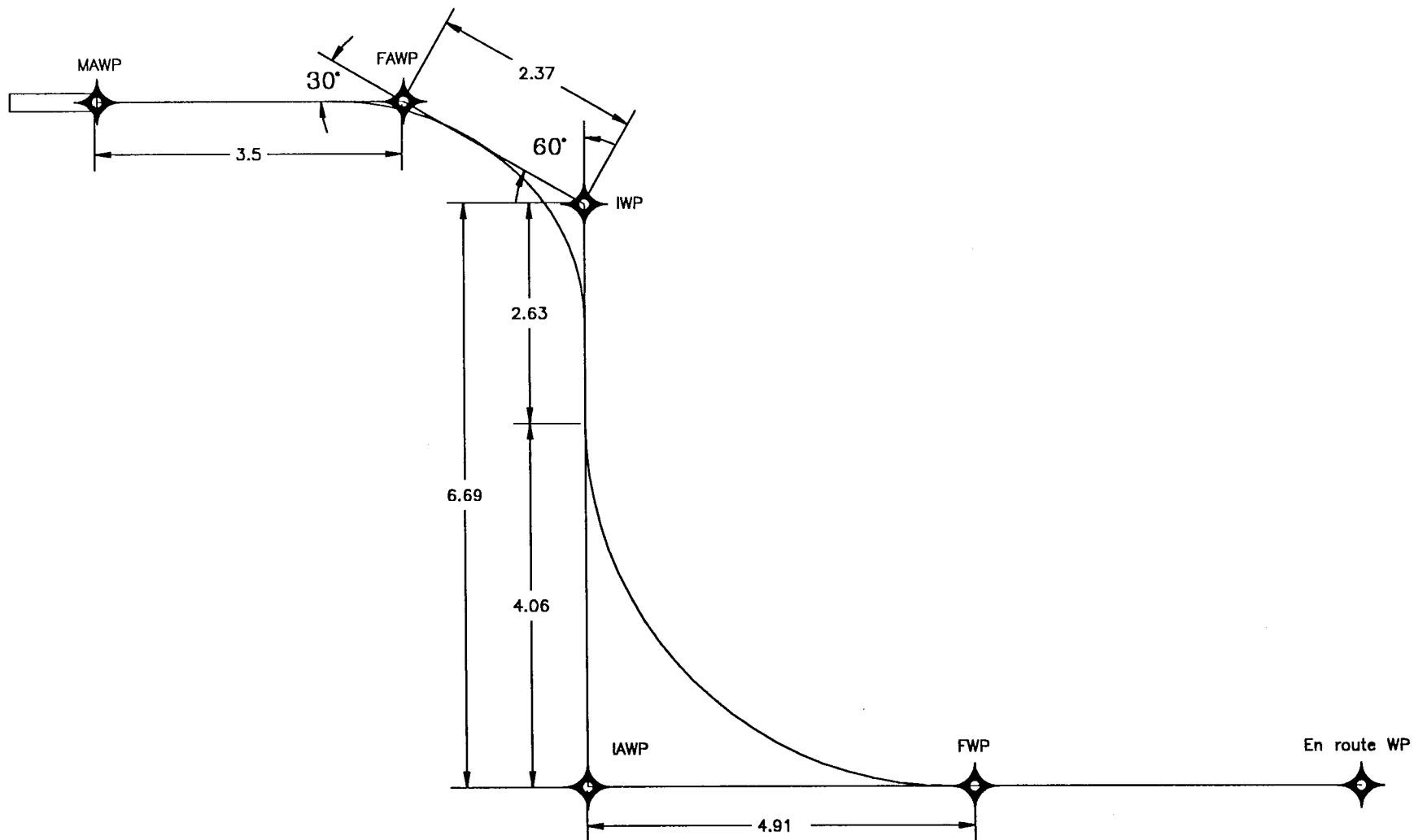




FIGURE 3. ENROUTE WAYPOINT FLY-OVER EXPANSION.

Paragraph 9c(2).

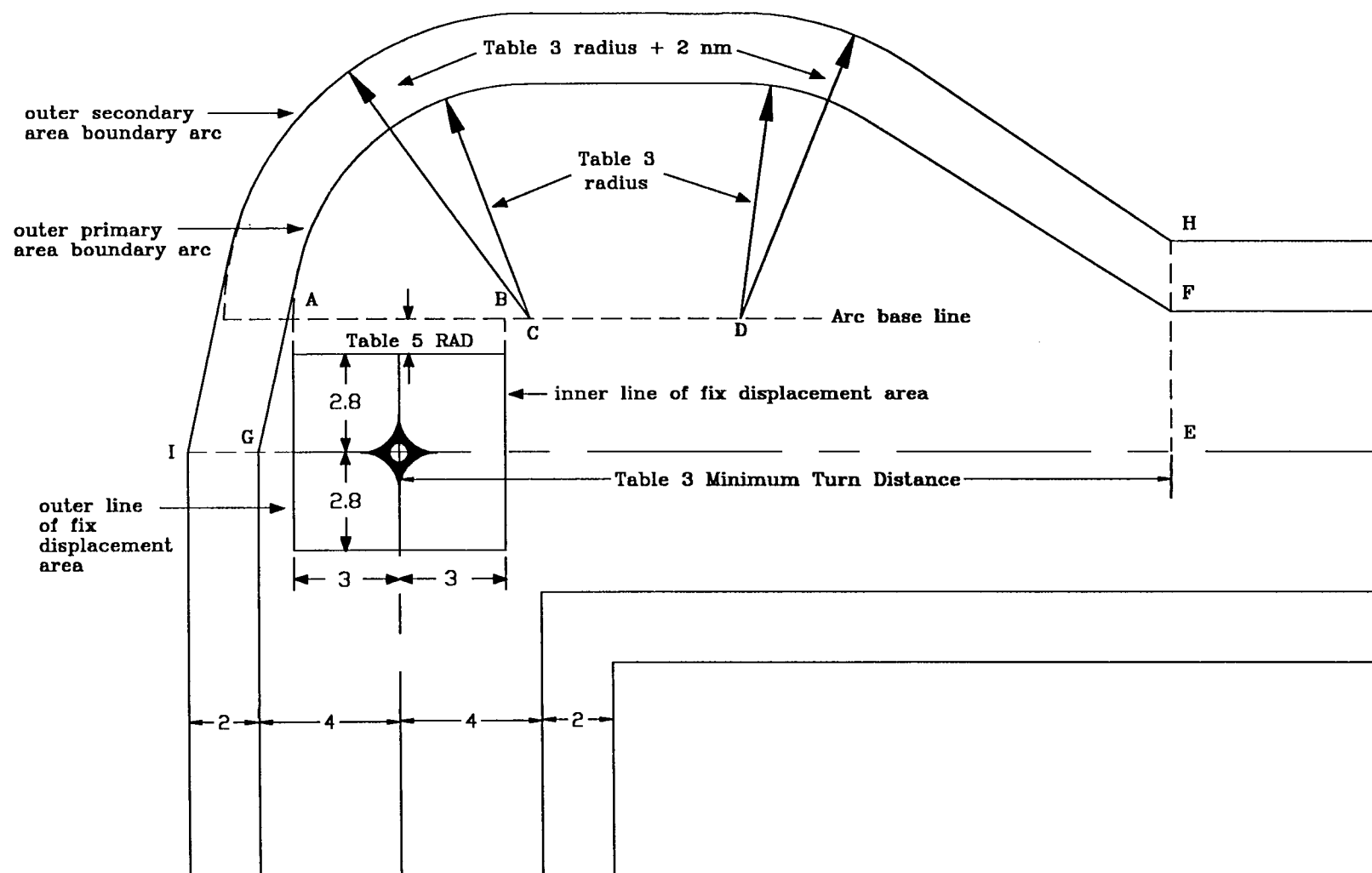


FIGURE 4. FMS NONPRECISION APPROACH CRITERIA, Paragraph 10a.

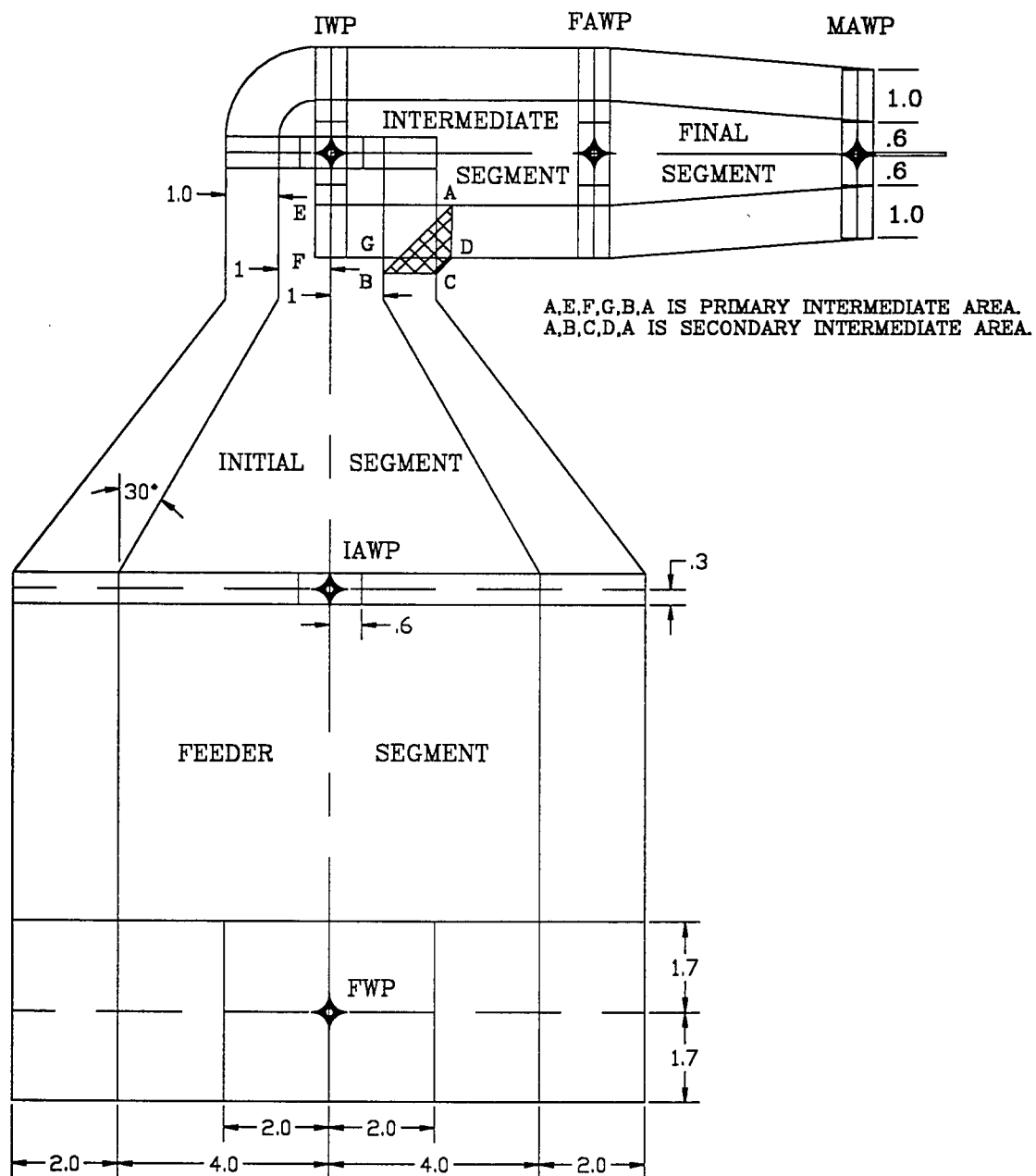


FIGURE 5. FMS NONPRECISION APPROACH CRITERIA,  
SHORT SEGMENT LENGTHS. Paragraph 10a.

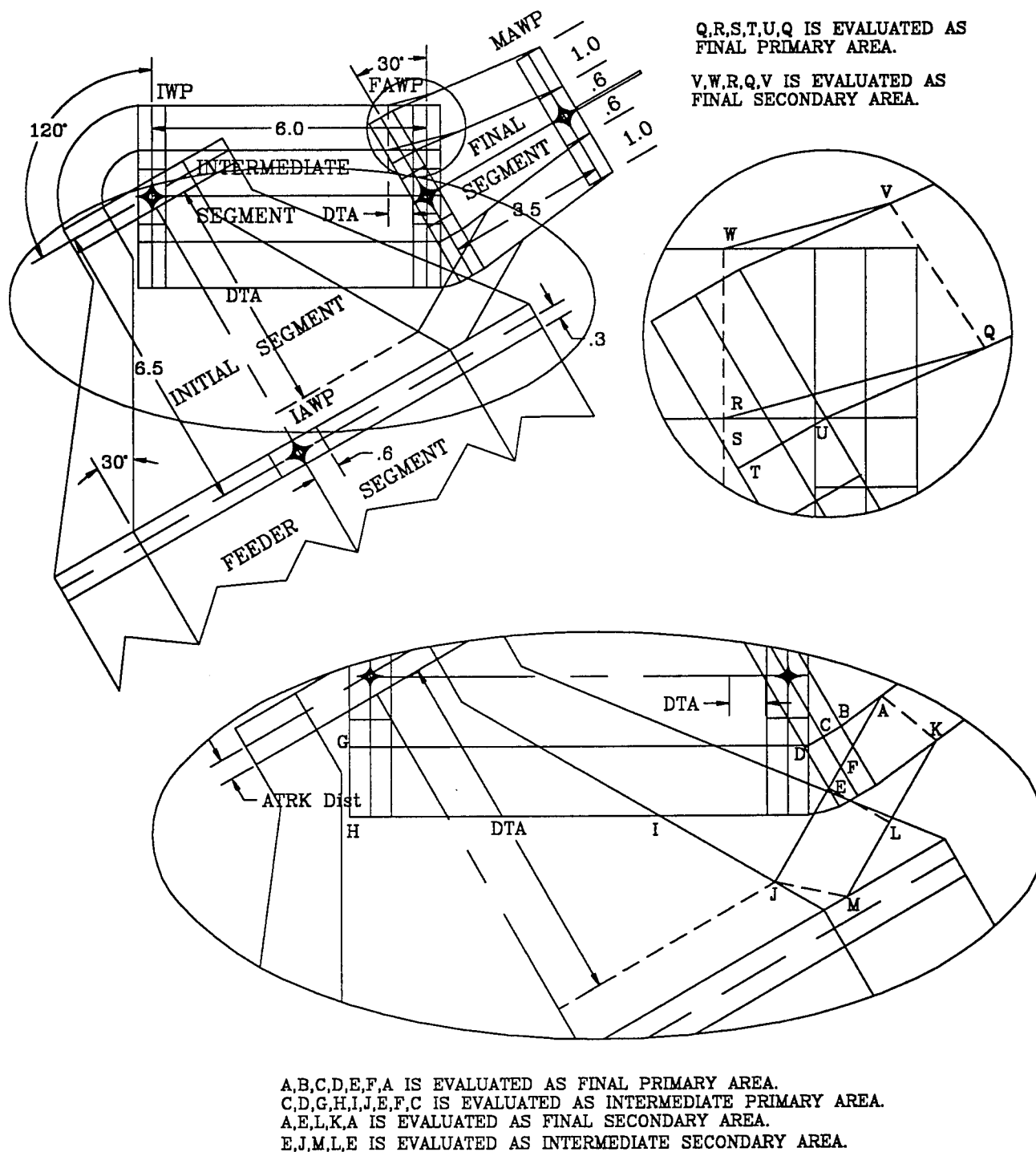


FIGURE 6. SEGMENTED PATH INITIAL SEGMENT.

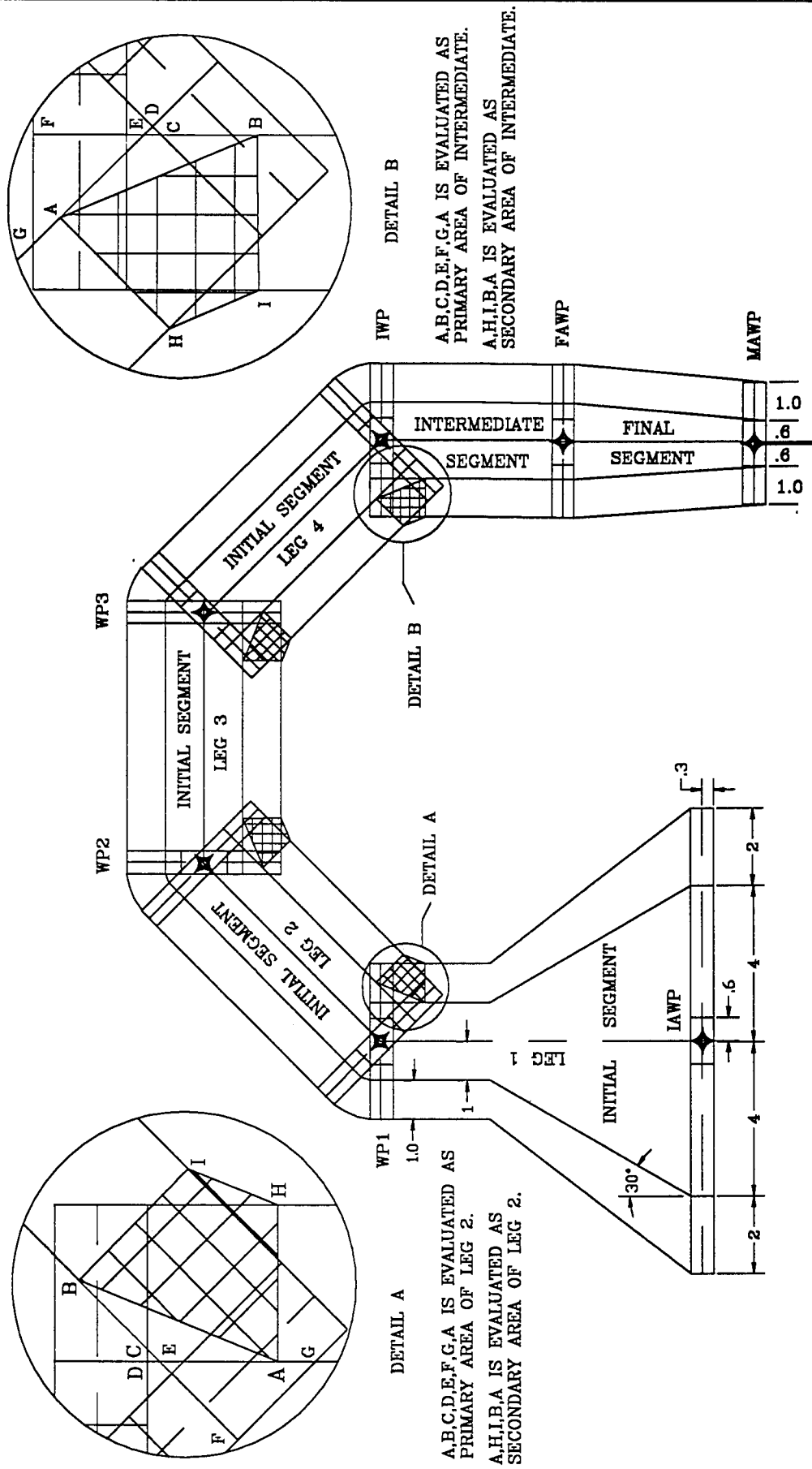


FIGURE 7. FINAL APPROACH SEGMENT, Paragraph 10d(2).

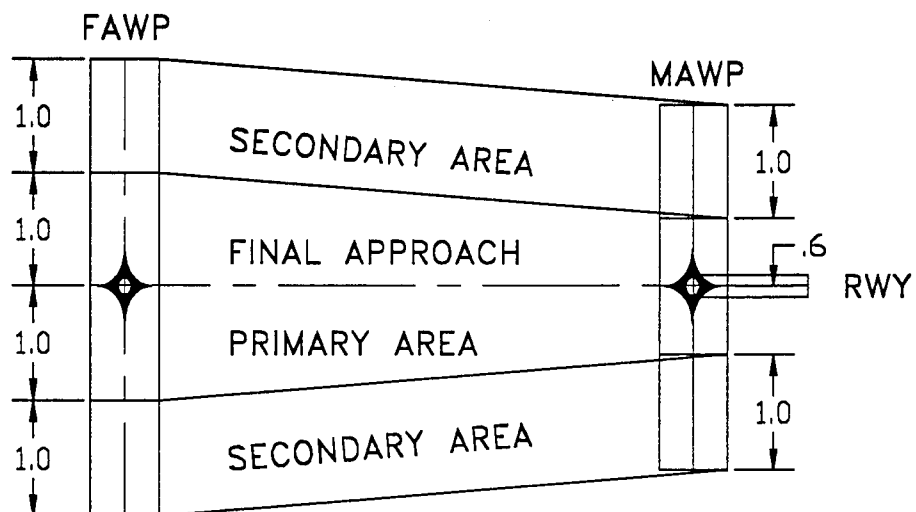


FIGURE 8. EXTENSION OF FINAL APPROACH SEGMENT TO  
RUNWAY THRESHOLD, Paragraph 10d(2).

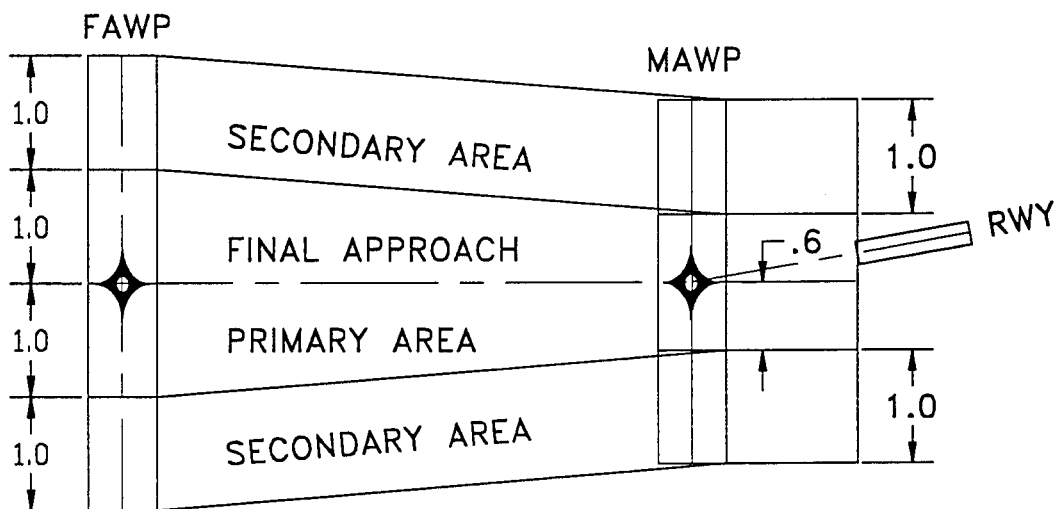


FIGURE 9. OBSTACLE RICH ENVIRONMENT ASSESSMENT.

Paragraphs 10e and 12e.

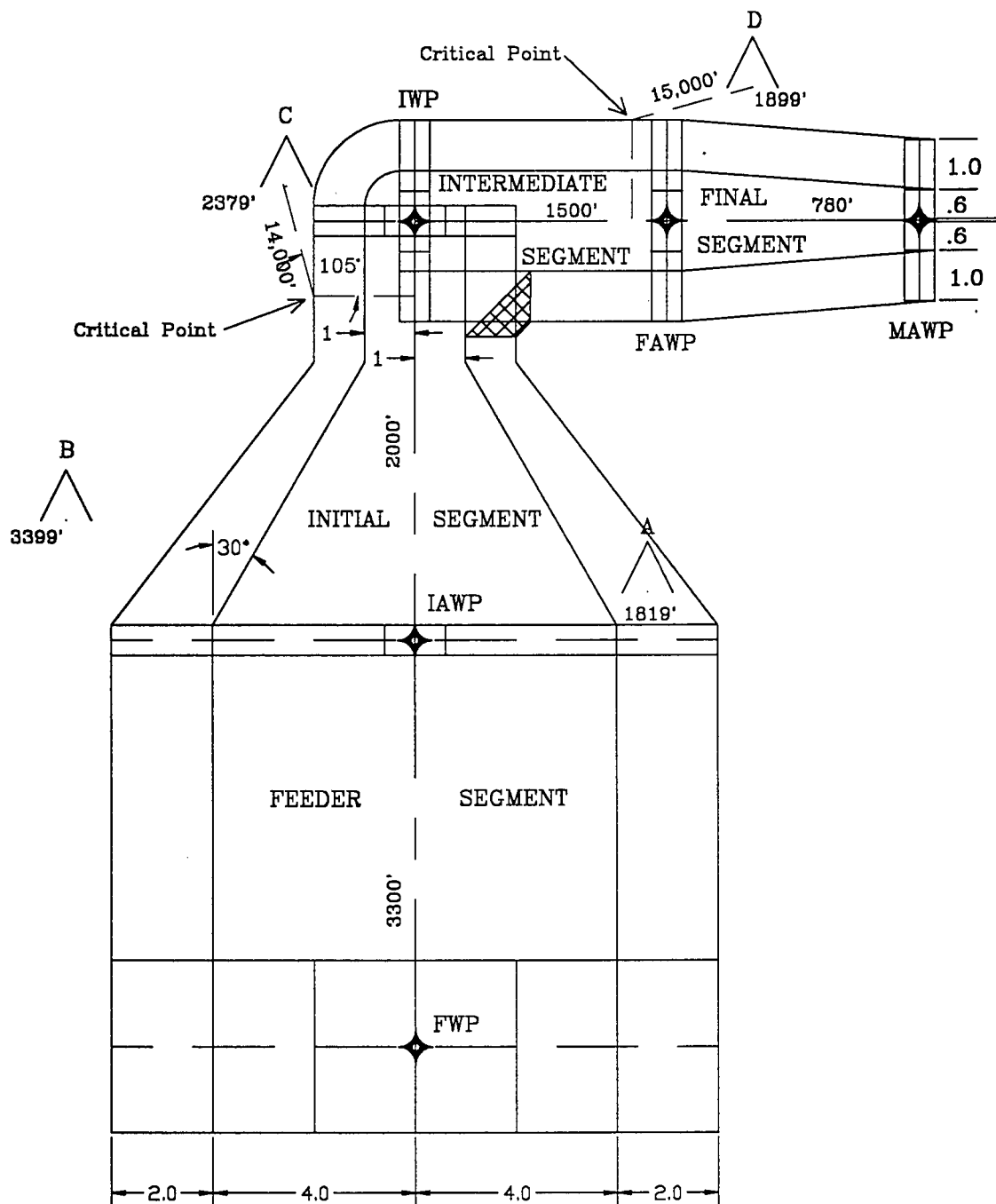


FIGURE 10. FMS TRANSITION TO ILS FINAL, SECTION 3.

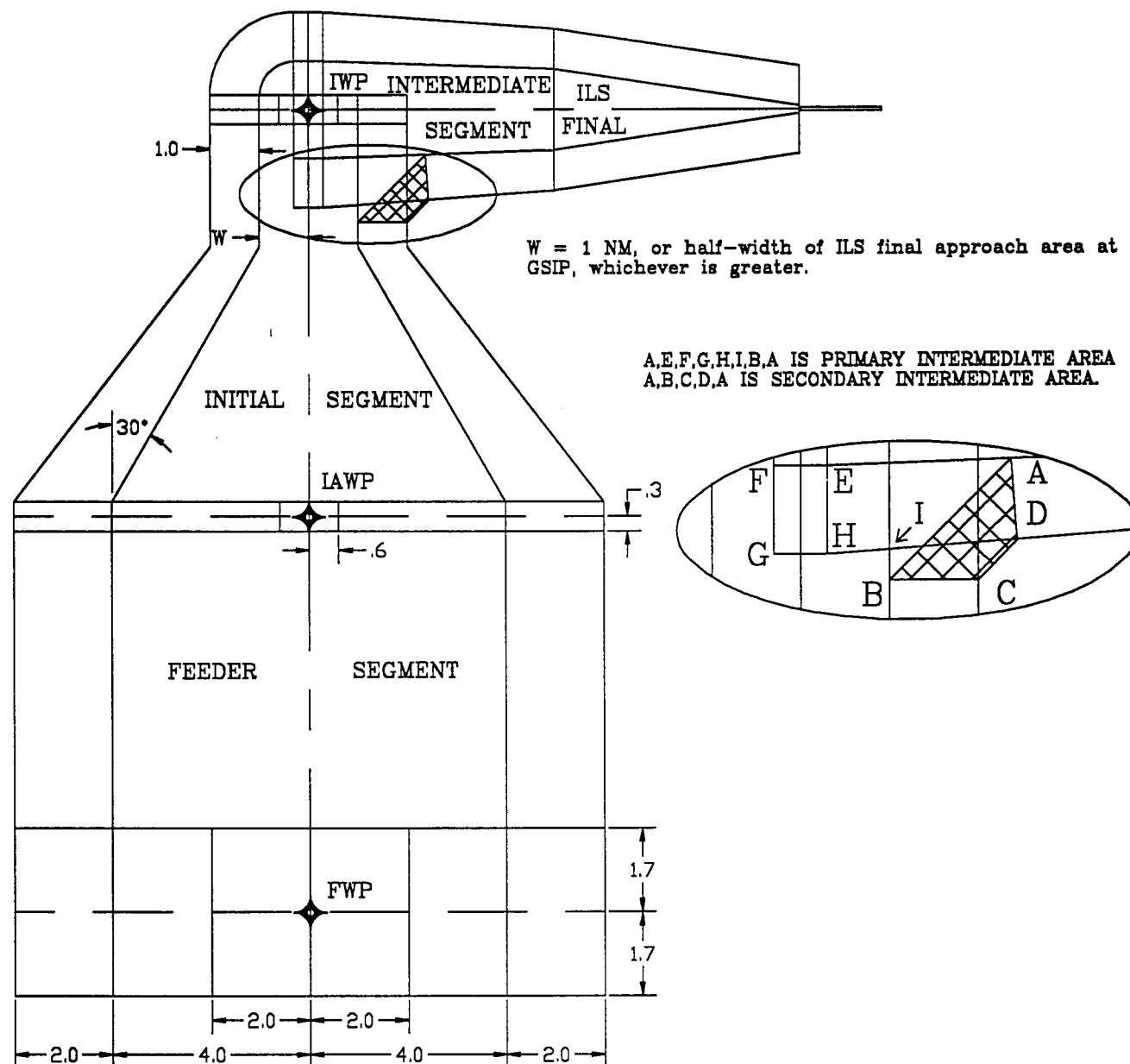
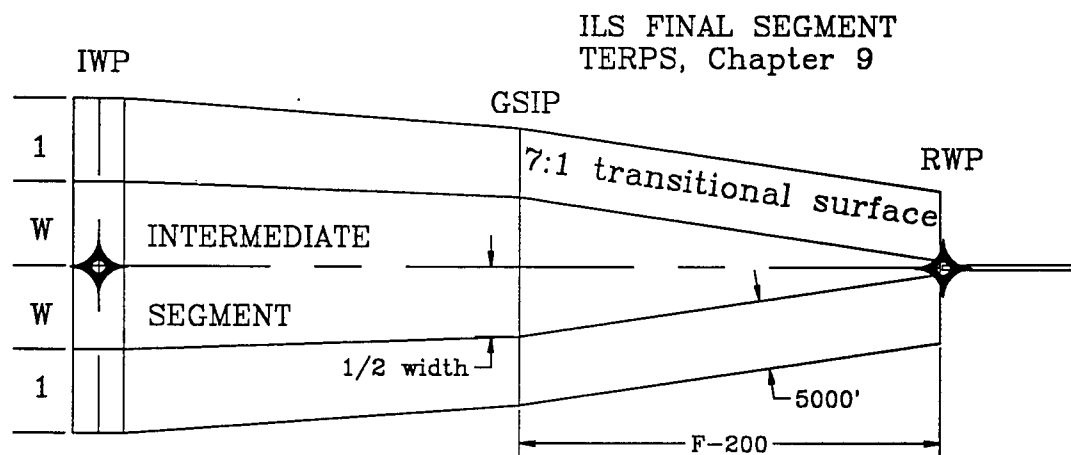




FIGURE 11. FMS INTERMEDIATE SEGMENT TO  
ILS FINAL SEGMENT, Paragraph 12c.



$F$  = distance from threshold to GSIP

$1/2 \text{ width} = 0.15 (F - 200') + 500'$

$W = 1 \text{ NM}$ , or half-width of ILS final approach area at GSIP whichever is greater.

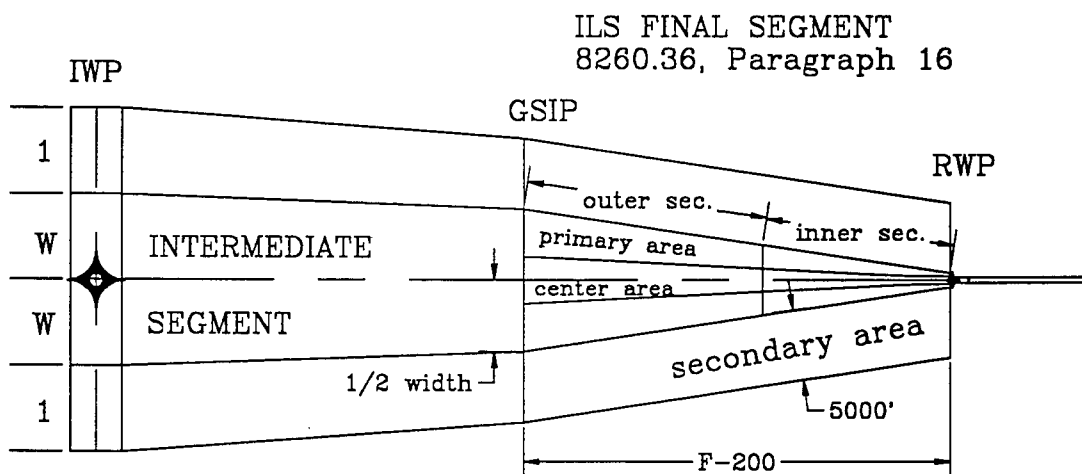
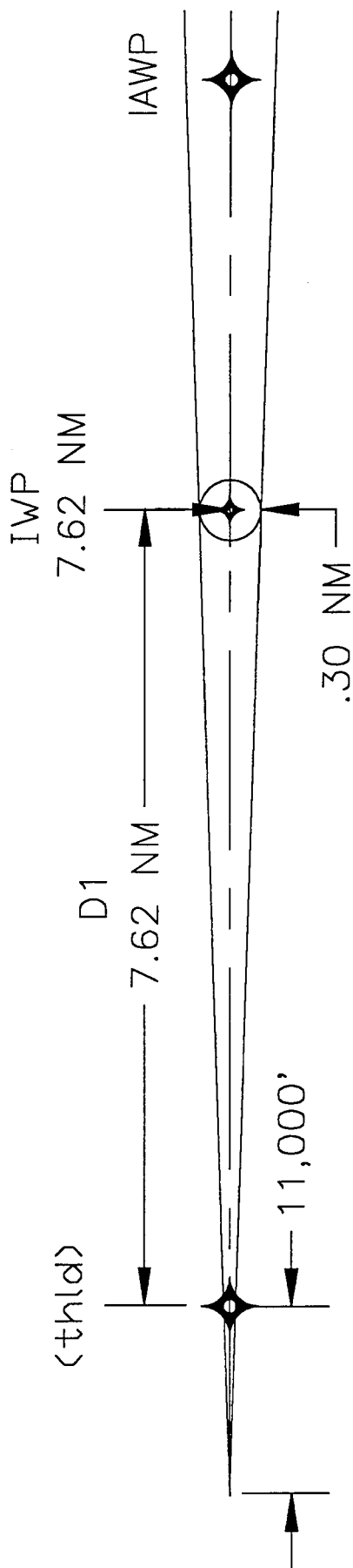


FIGURE 12. IWP PLACEMENT, EXAMPLE 1  
Paragraph 12c(7)(a).

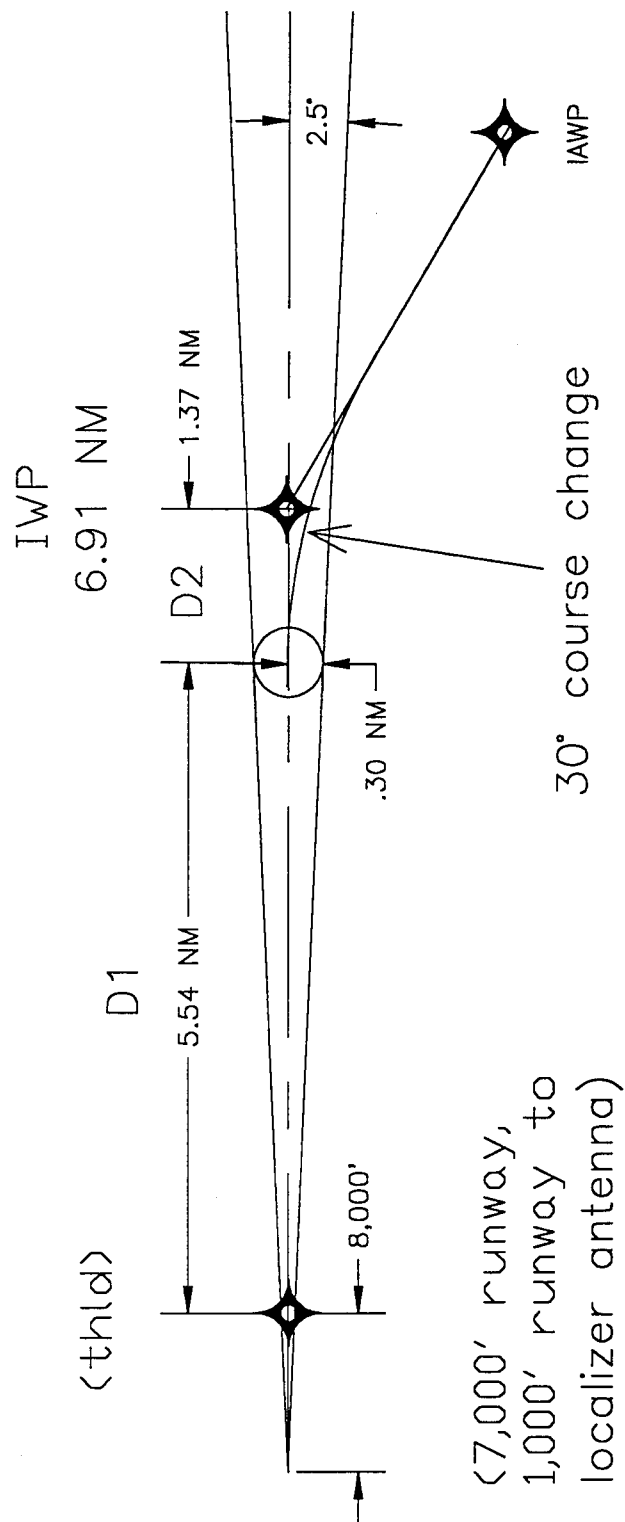


(10,000' runway,  
1,000' runway to  
localizer antenna)

$$D = 10,000' + 1,000' = 11,000'$$

$$D1 = 11,000' * ((.30/350) - .000164578) = 7.62 \text{ NM}$$

FIGURE 13. IWP PLACEMENT, EXAMPLE 2.  
Paragraph 12c(7)(b).



$$D = 7,000' + 1,000' = 8,000'$$

$$D1 = 8,000' * ((.30/350') - .000164578) = 5.54 \text{ NM}$$

$$D2 = \text{TABLE 2 MINIMUM TURN DISTANCE} = 1.37 \text{ NM}$$

FIGURE 14. IWP PLACEMENT, EXAMPLE 3.  
Paragraph 12c(7)(b).

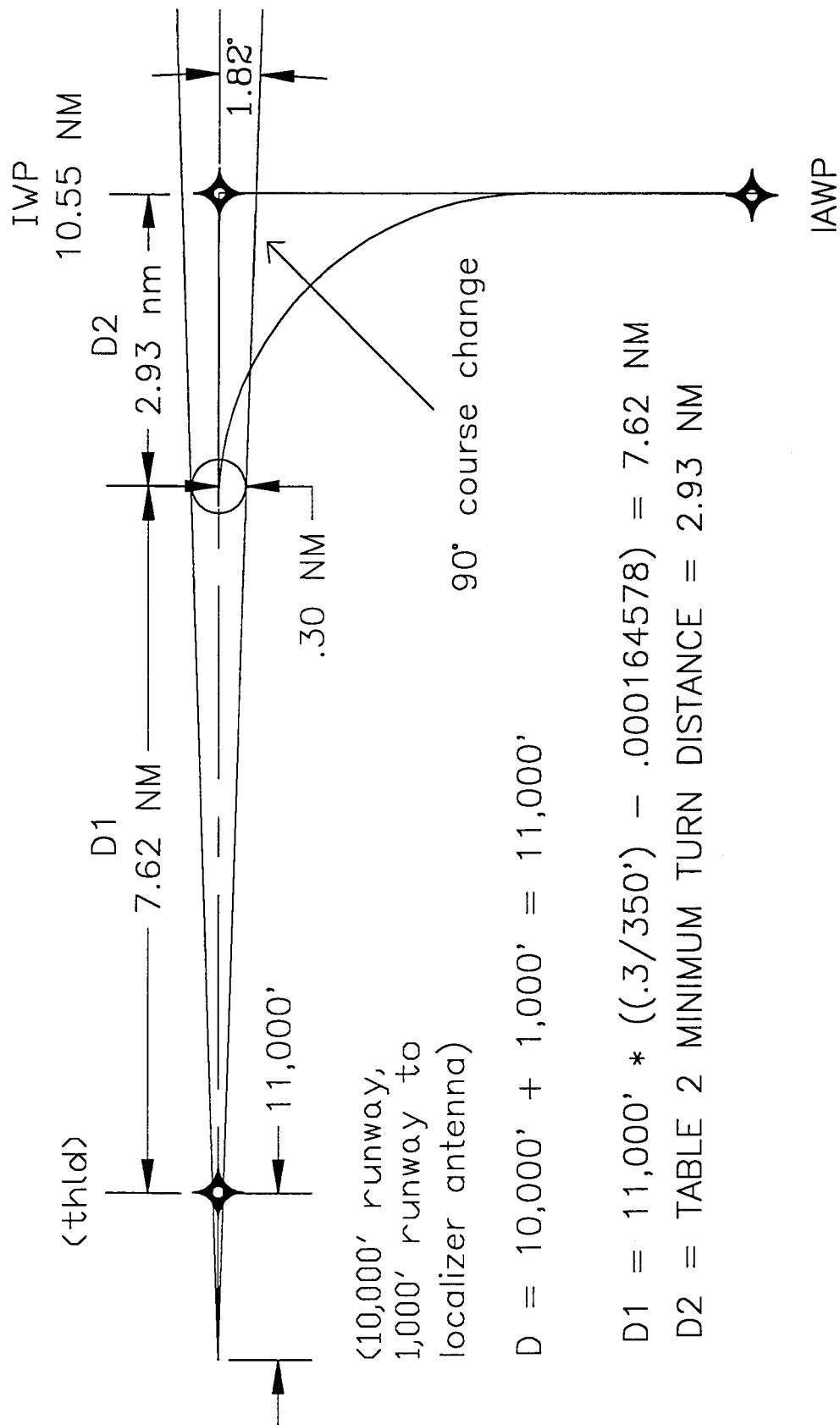


Figure 15. MINIMUM FIRST SEGMENT LENGTH.  
Paragraph 13a(1).

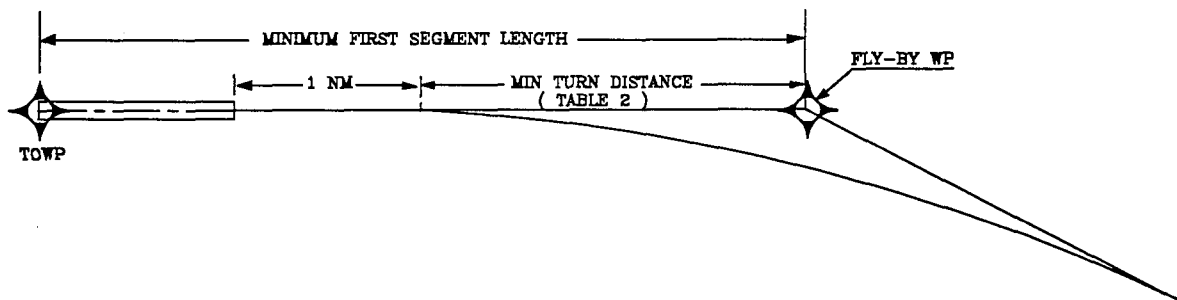


Figure 16. DEPARTURE AREA.  
Paragraph 13b(1).

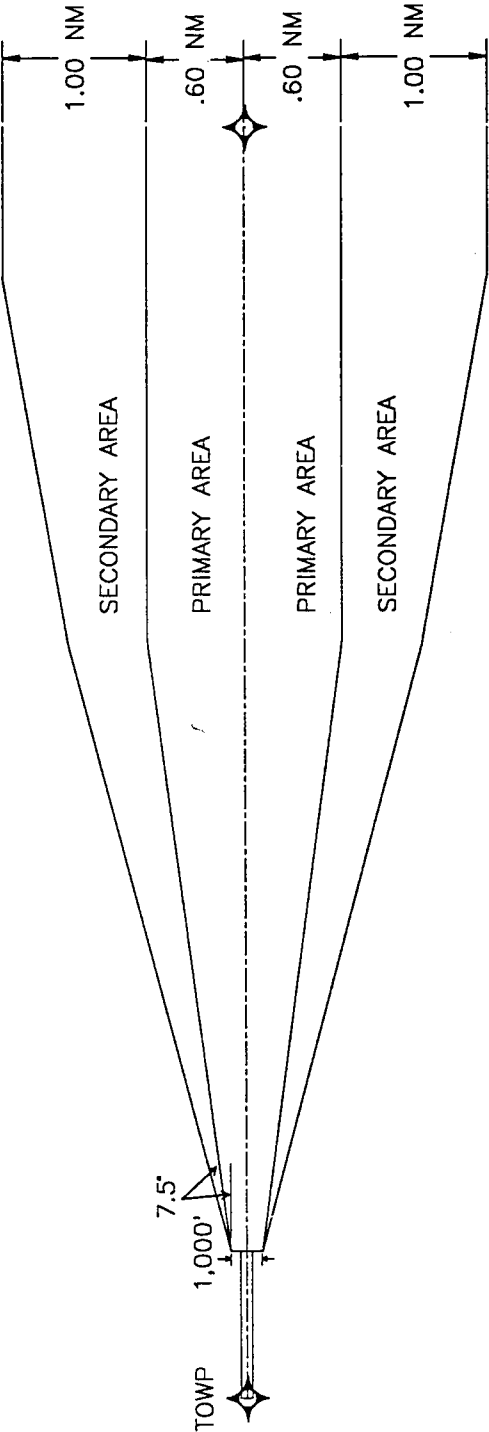


Figure 17. DEPARTURE AREA, FLY-BY WAYPOINT, SPLAY INCOMPLETE.  
Paragraph 13b(1)(a).

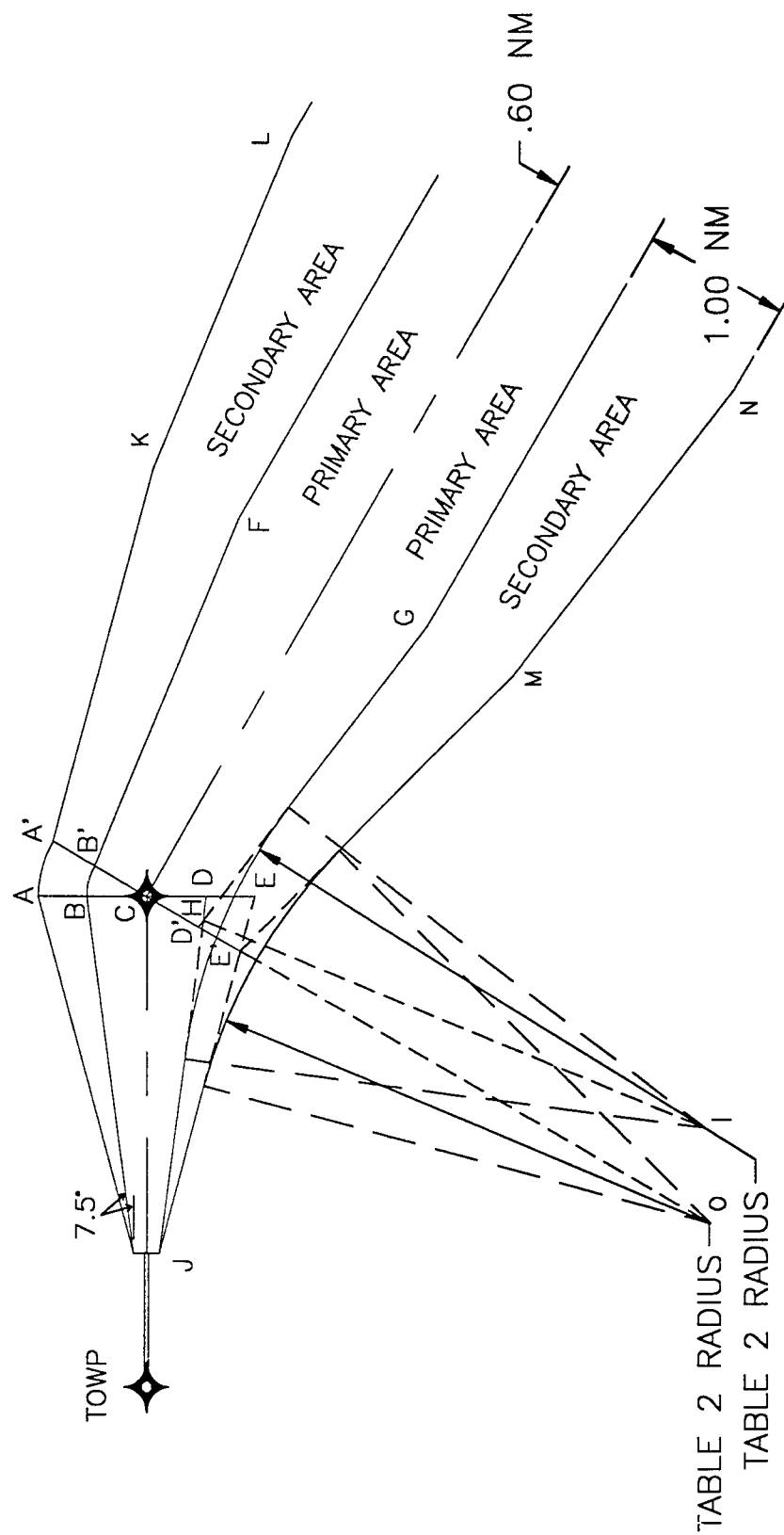


Figure 18. DEPARTURE AREA, FLY-BY WAYPOINT, SPLAY COMPLETE.  
Paragraph 13b(1)(b).

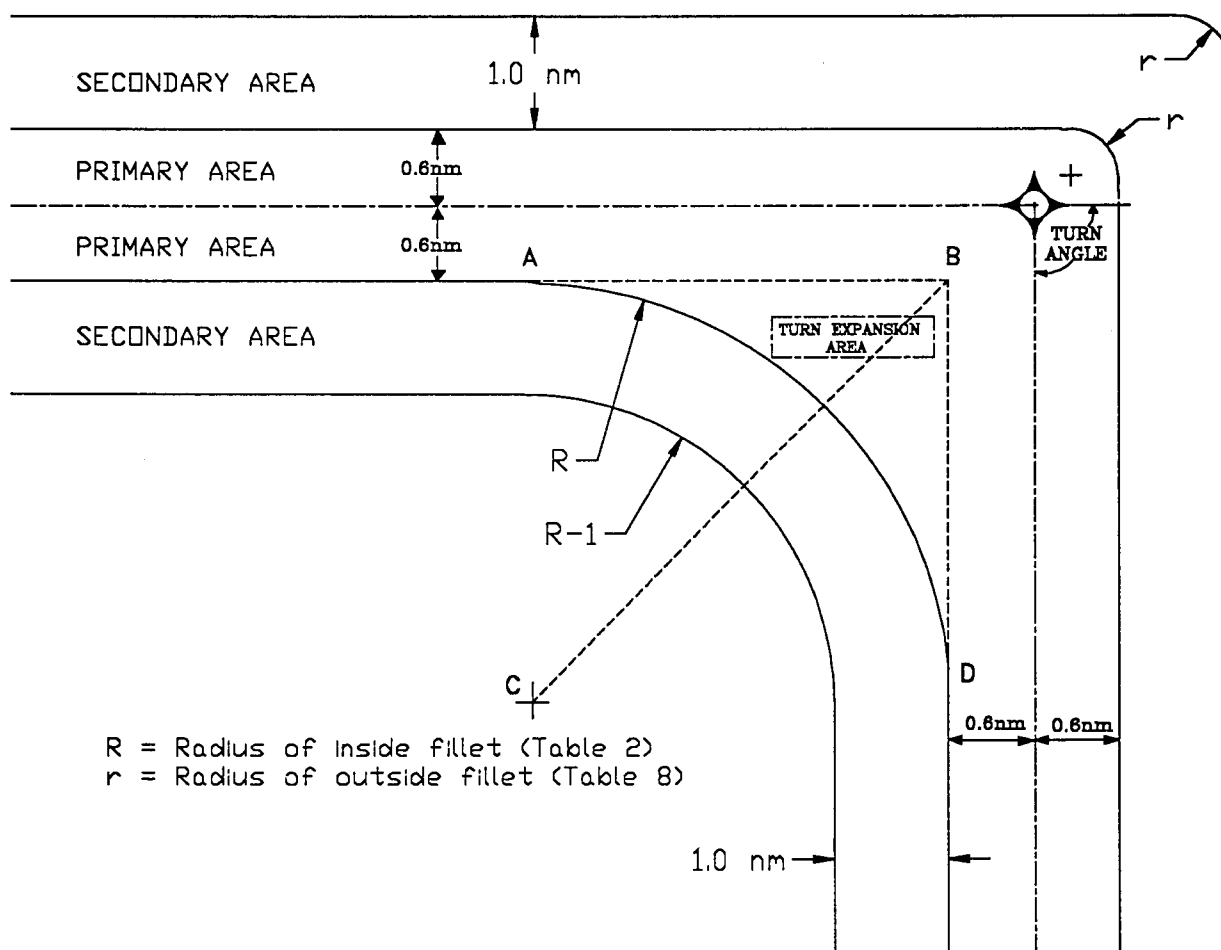




Figure 19. DEPARTURE AREA – TURN ANGLES LESS THAN 10 DEGREES.  
Paragraph 13b(1)(b).

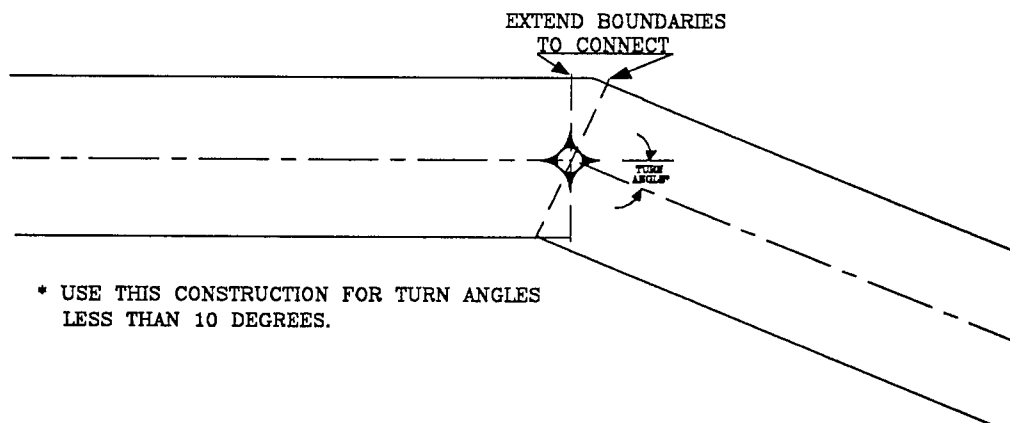


Figure 20. DEPARTURE AREA, FLY-OVER WAYPOINT, SPLAY INCOMPLETE. Paragraph 13b(1)(c).

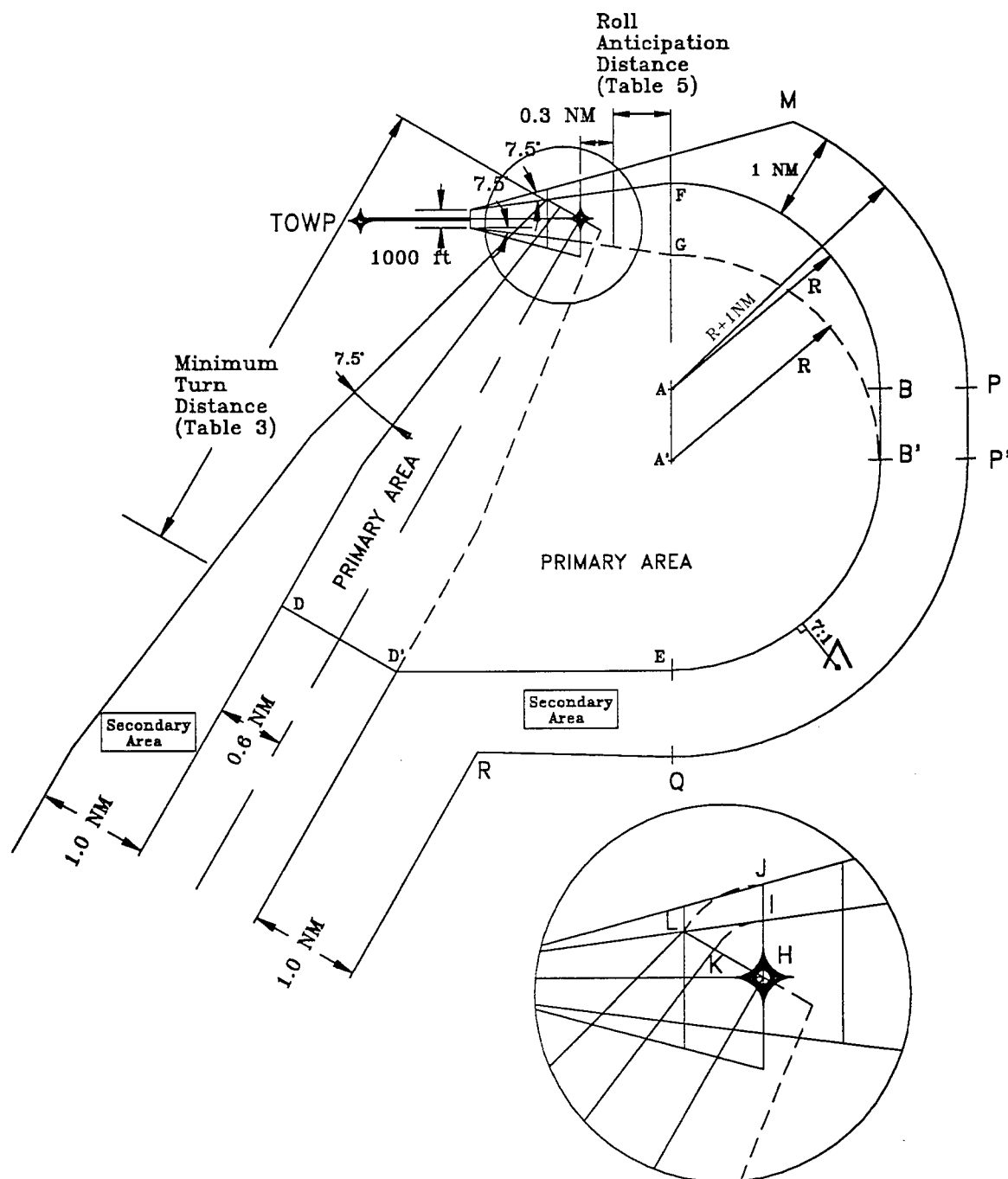


Figure 21. DEPARTURE AREA, FLY-OVER WAYPOINT, SPLAY COMPLETE.  
Paragraph 13b(1)(d).

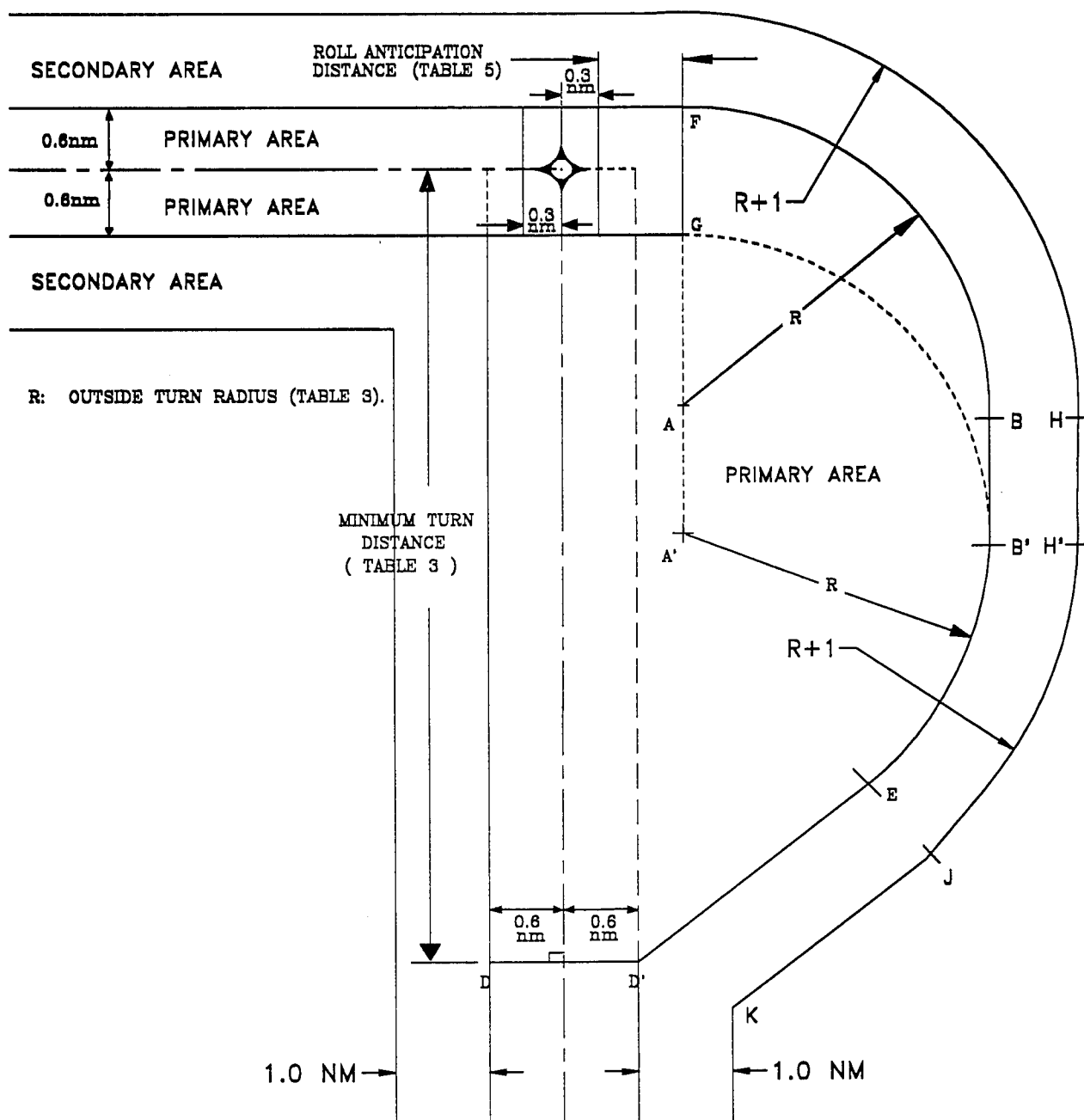
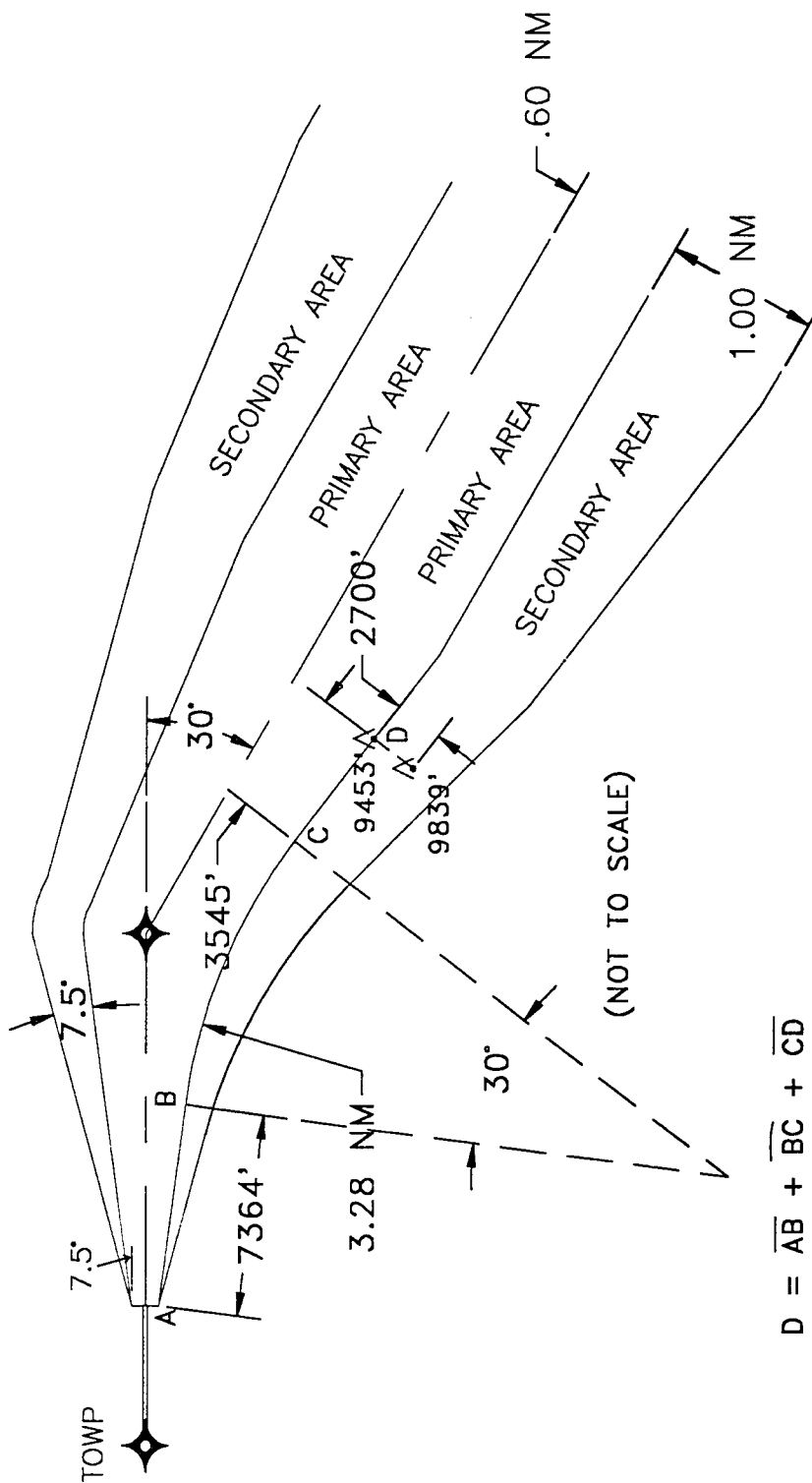


Figure 22. CLIMB GRADIENT COMPUTATION.  
Paragraph 13c(3).



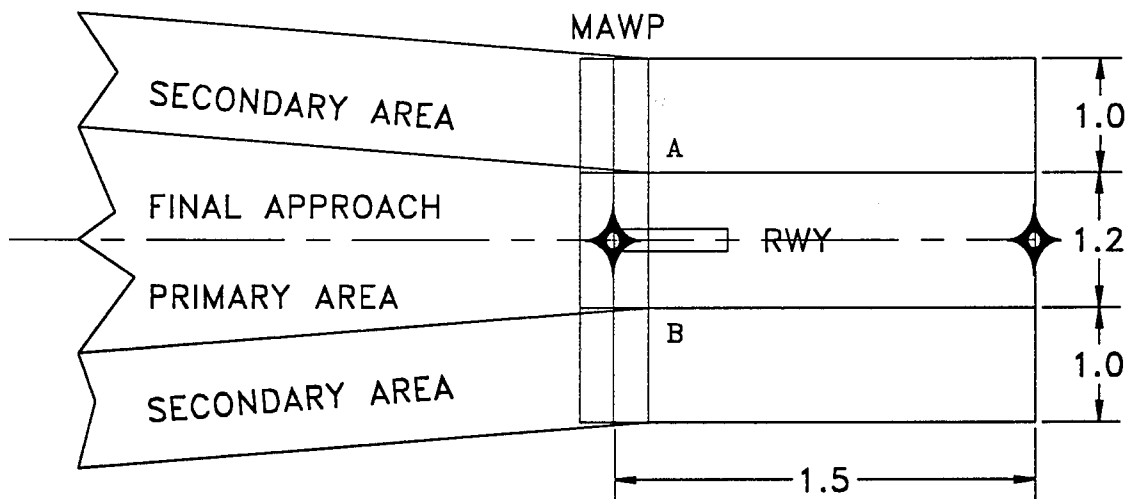
$$D = \overline{AB} + \overline{BC} + \overline{CD}$$

$$\overline{BC} = (\text{radius in feet}) * (\text{turn angle}) * (.017453)$$

$$= (19929.6) * (30) * (.017453) = 10,435'$$

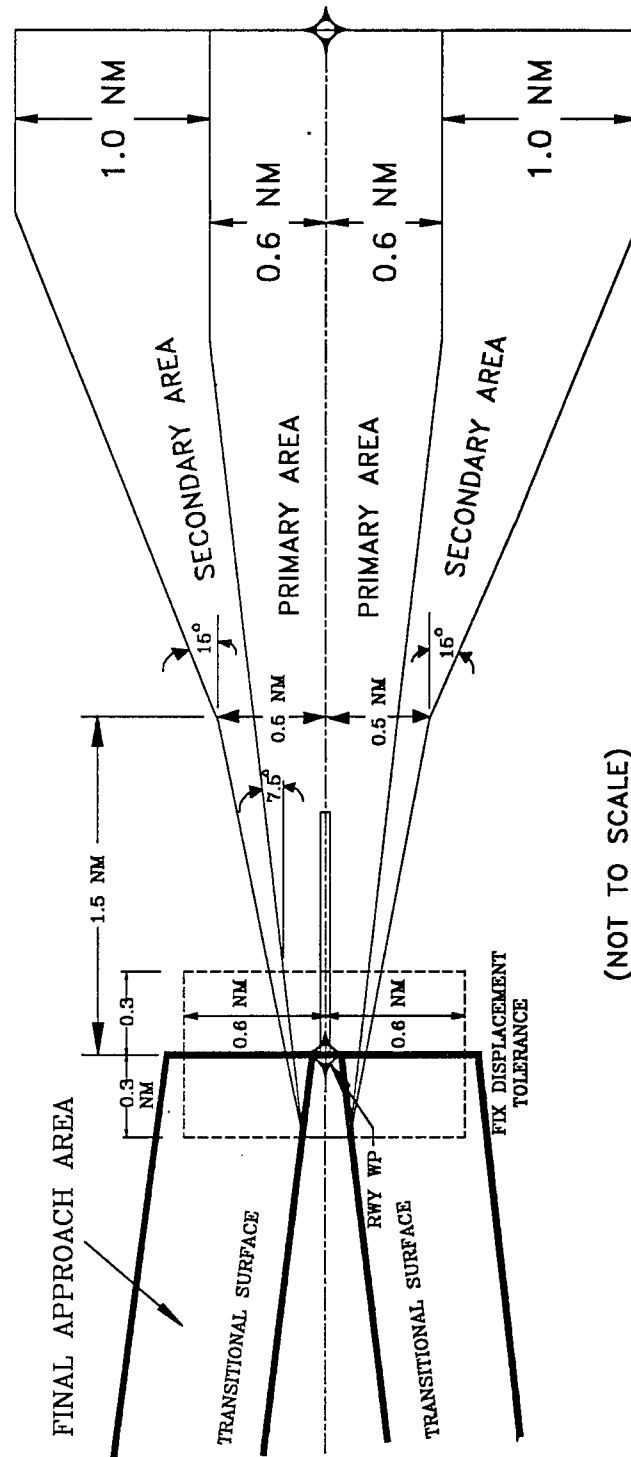
$$D = 7364' + 10435' + 3545' = 21,344' = 3.51 \text{ NM}$$

FIGURE 23. FMS NONPRECISION APPROACH MISSED APPROACH AREA.  
Paragraphs 14c(1)(a) and 14c(2)(a).



(not to scale)

Figure 24. FMS MISSED APPROACH AREA  
FOR LOCALIZER FINAL APPROACH.  
Paragraphs 14c(1)(b) and 14c(2)(b).



(NOT TO SCALE)

Figure 25. FMS MISSED APPROACH AREA  
FOR ILS FINAL APPROACH.  
Paragraphs 14c(1)(c) and 14c(2)(c).

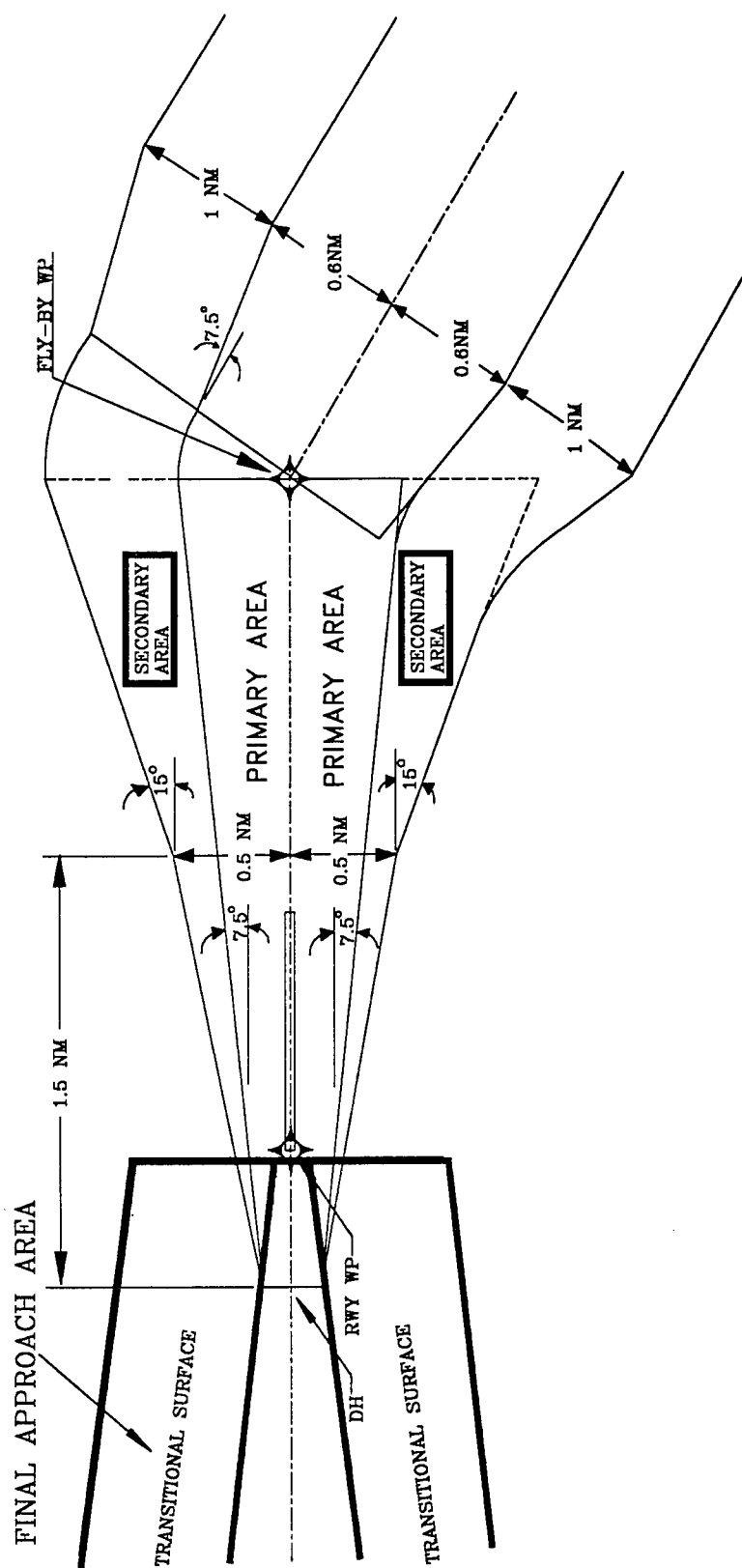


Figure 26. FMS MISSED APPROACH AREA  
FOR ILS OFFSET 3 DEGREES OR LESS.

Paragraphs 14c(1)(d) and 14c(2)(d).

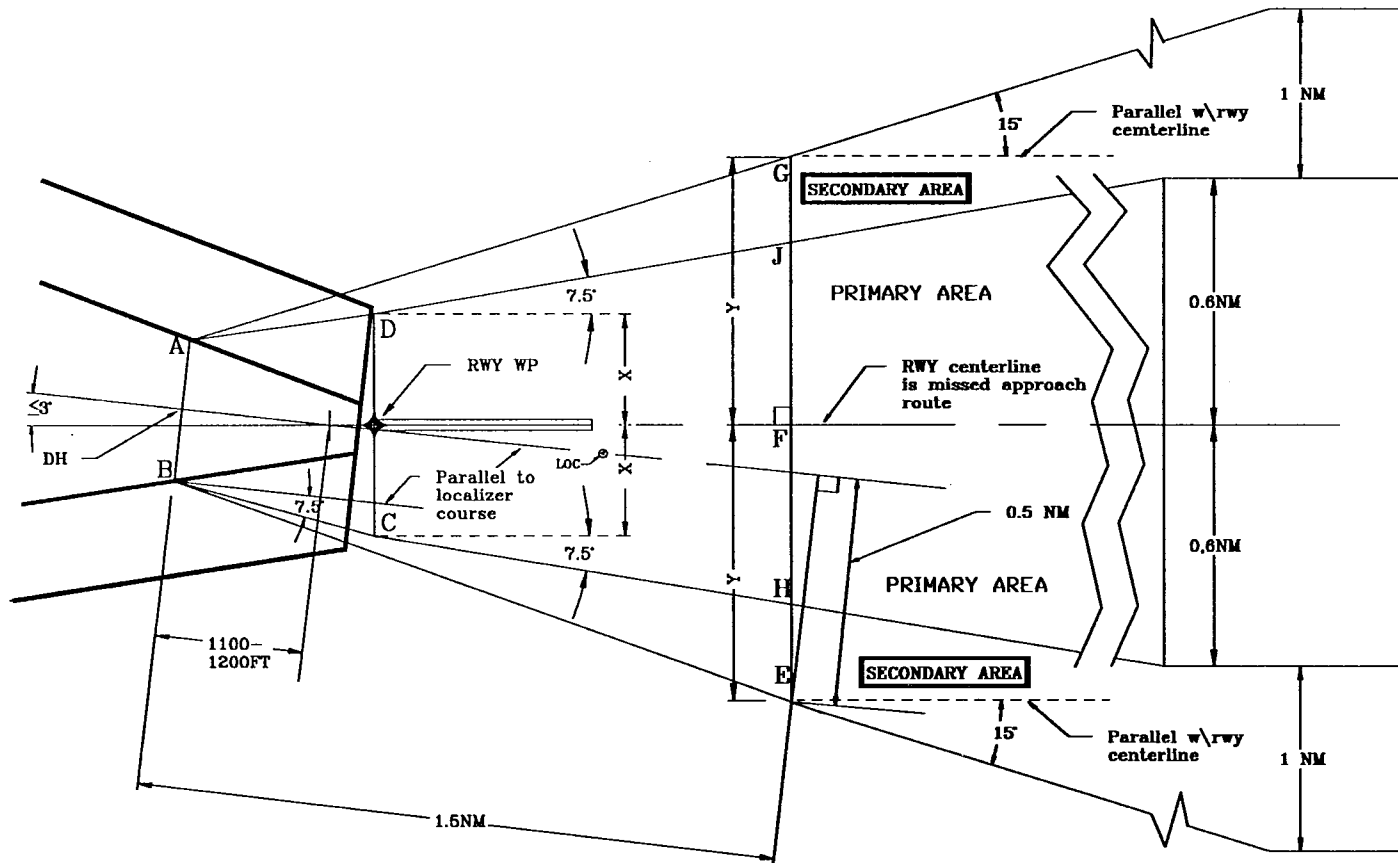




Figure 27. FMS MISSED APPROACH AREA  
FOR MLS FINAL APPROACH.  
Paragraphs 14c(1)(c) and 14c(2)(c).

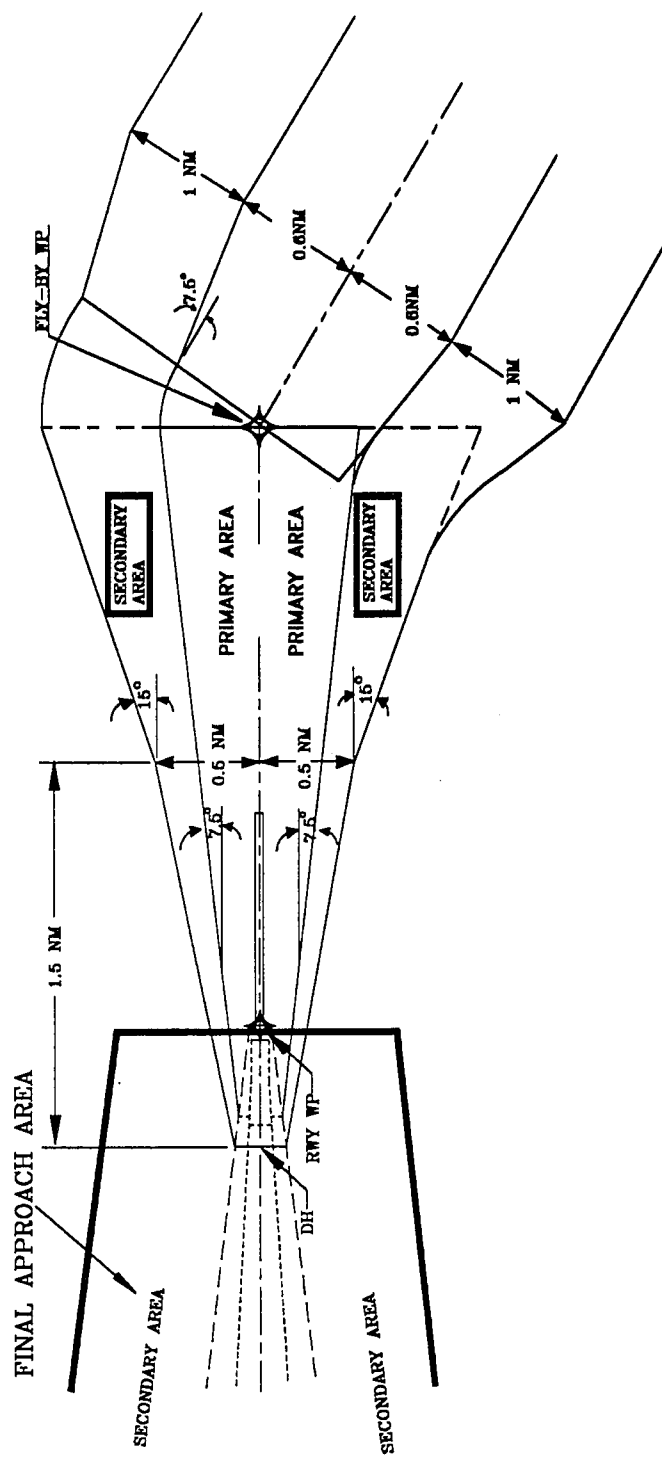
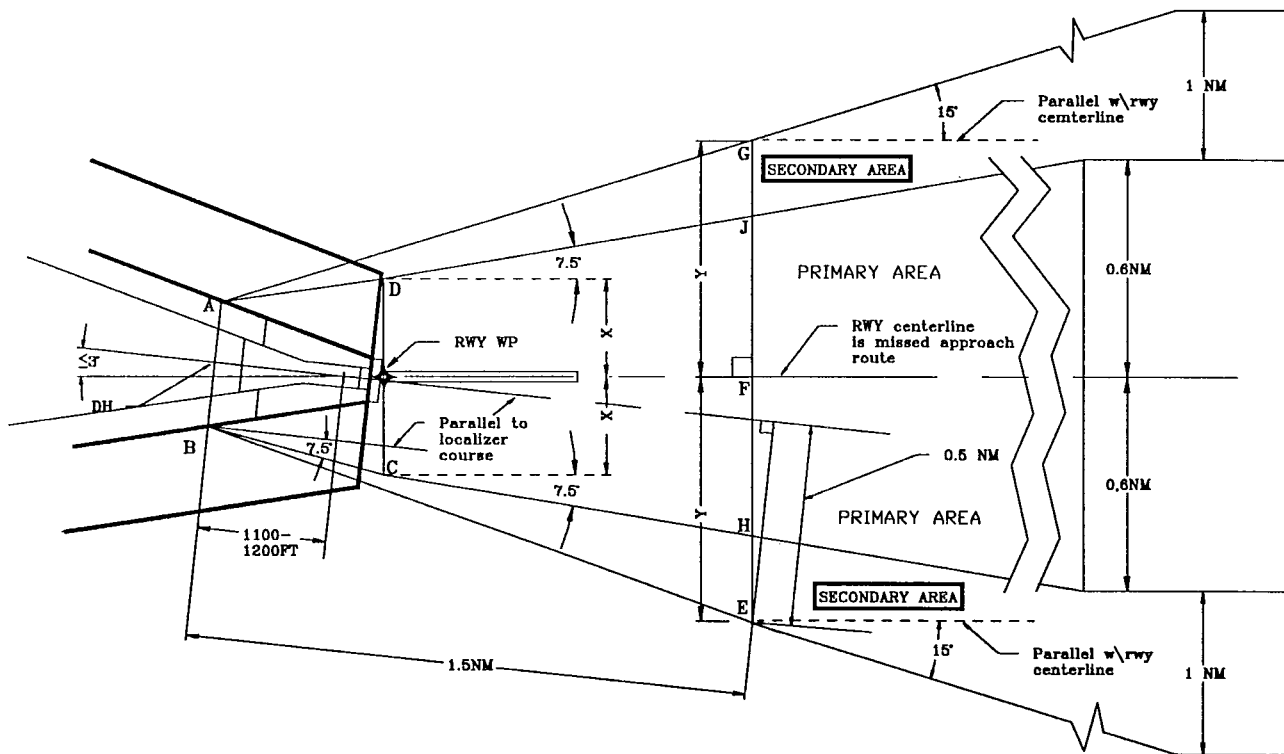


Figure 28. MLS MISSED APPROACH AREA  
OFFSET 3 DEGREES OR LESS.

Paragraphs 14c(1)(d) and 14c(2)(d).



**TABLE 1**  
**WAYPOINT DESIGN CRITERIA**

| WAYPOINT | TYPE     | ATRK<br>(NM) | XTRK<br>(NM) | FLY-BY<br>ALLOWED | FLY-OVER<br>ALLOWED |
|----------|----------|--------------|--------------|-------------------|---------------------|
| En route | En route | +/- 2.8      | +/- 3.0      | Yes               | Yes                 |
| FWP      | Terminal | +/- 1.7      | +/- 2.0      | Yes               | Yes                 |
| IAWP     | Approach | +/- 0.3      | +/- 0.6      | Yes               | No                  |
| IWP      | Approach | +/- 0.3      | +/- 0.6      | Yes               | No                  |
| FAWP     | Approach | +/- 0.3      | +/- 0.6      | Yes               | No                  |
| MAWP     | Approach | +/- 0.3      | +/- 0.6      | No                | Yes                 |
| MAHWP    | Approach | +/- 0.3      | +/- 0.6      | Yes               | Yes                 |

**TABLE 2**  
**FLY-BY WAYPOINT MINIMUM TURN DISTANCE AND RADIUS**

| TURN<br>ANGLE<br>(degrees) | INSIDE TURN EXPANSION |                          |                |                          |                |                          |                |                          |                |                          |
|----------------------------|-----------------------|--------------------------|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|
|                            | 160 KIAS              |                          | 175 KIAS       |                          | 220 KIAS       |                          | 250 KIAS       |                          | 310 KIAS       |                          |
|                            | RADIUS<br>(nm)        | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) |
| 10                         | 10.04                 | 0.99                     | 11.58          | 1.13                     | 16.46          | 1.59                     | 20.24          | 1.93                     | 37.31          | 3.48                     |
| 15                         | 6.67                  | 1.05                     | 7.64           | 1.19                     | 10.94          | 1.66                     | 13.45          | 2.01                     | 24.79          | 3.59                     |
| 20                         | 4.98                  | 1.11                     | 5.71           | 1.25                     | 8.17           | 1.73                     | 10.04          | 2.09                     | 18.51          | 3.70                     |
| 25                         | 3.96                  | 1.16                     | 4.54           | 1.31                     | 6.50           | 1.80                     | 7.99           | 2.17                     | 14.72          | 3.81                     |
| 30                         | 3.28                  | 1.22                     | 3.76           | 1.37                     | 5.37           | 1.88                     | 6.61           | 2.25                     | 12.18          | 3.92                     |
| 35                         | 3.00                  | 1.32                     | 3.43           | 1.48                     | 4.91           | 2.02                     | 6.04           | 2.43                     | 11.14          | 4.23                     |
| 40                         | 2.76                  | 1.41                     | 3.16           | 1.58                     | 4.52           | 2.16                     | 5.56           | 2.59                     | 10.25          | 4.50                     |
| 45                         | 2.55                  | 1.49                     | 2.92           | 1.67                     | 4.18           | 2.29                     | 5.14           | 2.74                     | 9.48           | 4.76                     |
| 50                         | 2.37                  | 1.57                     | 2.72           | 1.76                     | 3.89           | 2.40                     | 4.78           | 2.88                     | 8.81           | 5.00                     |
| 55                         | 2.21                  | 1.64                     | 2.53           | 1.85                     | 3.63           | 2.52                     | 4.46           | 3.02                     | 8.22           | 5.23                     |
| 60                         | 2.07                  | 1.72                     | 2.37           | 1.93                     | 3.39           | 2.63                     | 4.17           | 3.15                     | 7.69           | 5.45                     |
| 65                         | 2.07                  | 1.84                     | 2.37           | 2.07                     | 3.39           | 2.83                     | 4.17           | 3.40                     | 7.69           | 5.91                     |
| 70                         | 2.07                  | 1.97                     | 2.37           | 2.22                     | 3.39           | 3.04                     | 4.17           | 3.66                     | 7.69           | 6.39                     |
| 75                         | 2.07                  | 2.11                     | 2.37           | 2.38                     | 3.39           | 3.27                     | 4.17           | 3.94                     | 7.69           | 6.91                     |
| 80                         | 2.07                  | 2.26                     | 2.37           | 2.55                     | 3.39           | 3.52                     | 4.17           | 4.24                     | 7.69           | 7.46                     |
| 85                         | 2.07                  | 2.42                     | 2.37           | 2.73                     | 3.39           | 3.78                     | 4.17           | 4.56                     | 7.69           | 8.05                     |
| 90                         | 2.07                  | 2.59                     | 2.37           | 2.93                     | 3.39           | 4.06                     | 4.17           | 4.91                     | 7.69           | 8.70                     |
| 95                         | 2.07                  | 2.78                     | 2.37           | 3.15                     | 3.39           | 4.37                     | 4.17           | 5.29                     | 7.69           | 9.40                     |
| 100                        | 2.07                  | 2.99                     | 2.37           | 3.38                     | 3.39           | 4.71                     | 4.17           | 5.71                     | 7.69           | 10.17                    |
| 105                        | 2.07                  | 3.22                     | 2.37           | 3.65                     | 3.39           | 5.09                     | 4.17           | 6.18                     | 7.69           | 11.03                    |
| 110                        | 2.07                  | 3.48                     | 2.37           | 3.94                     | 3.39           | 5.51                     | 4.17           | 6.70                     | 7.69           | 11.99                    |
| 115                        | 2.07                  | 3.77                     | 2.37           | 4.28                     | 3.39           | 5.99                     | 4.17           | 7.29                     | 7.69           | 13.07                    |
| 120                        | 2.07                  | 4.11                     | 2.37           | 4.66                     | 3.39           | 6.54                     | 4.17           | 7.96                     | 7.69           | 14.32                    |

NOTE: When turn angle falls between values in table, interpolate or use the next larger value.

9/7/84

12/5/95

**TABLE 3**  
**FLY-OVER WAYPOINT MINIMUM TURN DISTANCE AND RADIUS**

| TURN<br>ANGLE<br>(degrees) | OUTSIDE TURN EXPANSION |                          |                |                          |                |                          |                |                          |                |                          |
|----------------------------|------------------------|--------------------------|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|
|                            | 160 KIAS               |                          | 175 KIAS       |                          | 220 KIAS       |                          | 250 KIAS       |                          | 310 KIAS       |                          |
|                            | RADIUS<br>(nm)         | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) | RADIUS<br>(nm) | MIN TURN<br>DIST<br>(nm) |
| 10                         | 6.17                   | 4.33                     | 6.60           | 4.63                     | 7.86           | 5.60                     | 8.70           | 6.31                     | 11.67          | 9.20                     |
| 15                         | 4.08                   | 4.83                     | 4.35           | 5.19                     | 5.17           | 6.36                     | 5.70           | 7.20                     | 7.69           | 10.66                    |
| 20                         | 3.02                   | 5.15                     | 3.22           | 5.55                     | 3.80           | 6.84                     | 4.17           | 7.77                     | 7.69           | 11.57                    |
| 25                         | 2.38                   | 5.36                     | 2.53           | 5.78                     | 3.39           | 7.15                     | 4.17           | 8.13                     | 7.69           | 12.13                    |
| 30                         | 2.07                   | 5.49                     | 2.37           | 5.93                     | 3.39           | 7.34                     | 4.17           | 8.35                     | 7.69           | 12.45                    |
| 35                         | 2.07                   | 5.56                     | 2.37           | 6.01                     | 3.39           | 7.44                     | 4.17           | 8.47                     | 7.69           | 12.60                    |
| 40                         | 2.07                   | 5.59                     | 2.37           | 6.04                     | 3.39           | 7.48                     | 4.17           | 8.50                     | 7.69           | 13.61                    |
| 45                         | 2.07                   | 5.59                     | 2.37           | 6.04                     | 3.39           | 7.66                     | 4.17           | 8.96                     | 7.69           | 14.84                    |
| 50                         | 2.07                   | 5.77                     | 2.37           | 6.32                     | 3.39           | 8.18                     | 4.17           | 9.59                     | 7.69           | 16.00                    |
| 55                         | 2.07                   | 6.06                     | 2.37           | 6.65                     | 3.39           | 8.65                     | 4.17           | 10.18                    | 7.69           | 17.08                    |
| 60                         | 2.07                   | 6.33                     | 2.37           | 6.95                     | 3.39           | 9.09                     | 4.17           | 10.72                    | 7.69           | 18.07                    |
| 65                         | 2.07                   | 6.57                     | 2.37           | 7.23                     | 3.39           | 9.49                     | 4.17           | 11.21                    | 7.69           | 18.98                    |
| 70                         | 2.07                   | 6.79                     | 2.37           | 7.49                     | 3.39           | 9.85                     | 4.17           | 11.65                    | 7.69           | 19.79                    |
| 75                         | 2.07                   | 6.98                     | 2.37           | 7.71                     | 3.39           | 10.17                    | 4.17           | 12.04                    | 7.69           | 20.51                    |
| 80                         | 2.07                   | 7.15                     | 2.37           | 7.90                     | 3.39           | 10.44                    | 4.17           | 12.38                    | 7.69           | 21.13                    |
| 85                         | 2.07                   | 7.29                     | 2.37           | 8.06                     | 3.39           | 10.67                    | 4.17           | 12.66                    | 7.69           | 21.64                    |
| 90                         | 2.07                   | 7.40                     | 2.37           | 8.18                     | 3.39           | 10.85                    | 4.17           | 12.88                    | 7.69           | 22.06                    |
| 95                         | 2.07                   | 7.50                     | 2.37           | 8.30                     | 3.39           | 11.02                    | 4.17           | 13.09                    | 7.69           | 22.45                    |
| 100                        | 2.07                   | 7.64                     | 2.37           | 8.47                     | 3.39           | 11.26                    | 4.17           | 13.38                    | 7.69           | 22.97                    |
| 105                        | 2.07                   | 7.77                     | 2.37           | 8.61                     | 3.39           | 11.46                    | 4.17           | 13.63                    | 7.69           | 23.44                    |
| 110                        | 2.07                   | 7.88                     | 2.37           | 8.73                     | 3.39           | 11.64                    | 4.17           | 13.85                    | 7.69           | 23.84                    |
| 115                        | 2.07                   | 7.97                     | 2.37           | 8.84                     | 3.39           | 11.78                    | 4.17           | 14.03                    | 7.69           | 24.17                    |
| 120                        | 2.07                   | 8.04                     | 2.37           | 8.92                     | 3.39           | 11.90                    | 4.17           | 14.17                    | 7.69           | 24.43                    |

NOTE: When turn angle falls between values in table, interpolate or use the next larger value.

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**TABLE 4**  
**SEGMENT VS SPEED**

| SEGMENT  | TABLES 2, 3 & 5<br>SPEED (KIAS) |
|--|---------------------------------|
| Initial Approach   | 220                             |
| Intermediate Approach  | 175                             |
| All others (enroute,<br>feeder, missed approach,<br>departure) |                                 |
| At and below 10,000' MSL                                       | 250                             |
| Above 10,000' MSL  | 310                             |

TABLE 5

| TURN<br>ANGLE<br>(degrees) | ROLL ANTICIPATION DISTANCE (NM) |          |          |          |          |          |          |          |          |          |
|----------------------------|---------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                            | 160 KIAS                        |          | 175 KIAS |          | 220 KIAS |          | 250 KIAS |          | 310 KIAS |          |
|                            | Fly-by                          | Fly-over | Fly-by   | Fly-over | Fly-by   | Fly-over | Fly-by   | Fly-over | Fly-by   | Fly-over |
| 10                         | 0.11                            | 0.18     | 0.12     | 0.21     | 0.15     | 0.30     | 0.16     | 0.37     | 0.22     | 0.68     |
| 15                         | 0.17                            | 0.28     | 0.18     | 0.32     | 0.22     | 0.45     | 0.24     | 0.56     | 0.33     | 1.01     |
| 20                         | 0.23                            | 0.37     | 0.24     | 0.42     | 0.29     | 0.60     | 0.32     | 0.74     | 0.44     | 1.01     |
| 25                         | 0.28                            | 0.46     | 0.30     | 0.53     | 0.36     | 0.67     | 0.40     | 0.74     | 0.55     | 1.01     |
| 30                         | 0.34                            | 0.52     | 0.37     | 0.56     | 0.44     | 0.67     | 0.48     | 0.74     | 0.66     | 1.01     |
| 35                         | 0.37                            | 0.52     | 0.40     | 0.56     | 0.48     | 0.67     | 0.53     | 0.74     | 0.72     | 1.01     |
| 40                         | 0.40                            | 0.52     | 0.43     | 0.56     | 0.51     | 0.67     | 0.57     | 0.74     | 0.77     | 1.01     |
| 45                         | 0.43                            | 0.52     | 0.46     | 0.56     | 0.55     | 0.67     | 0.61     | 0.74     | 0.83     | 1.01     |
| 50                         | 0.46                            | 0.52     | 0.49     | 0.56     | 0.59     | 0.67     | 0.66     | 0.74     | 0.89     | 1.01     |
| 55                         | 0.49                            | 0.52     | 0.53     | 0.56     | 0.63     | 0.67     | 0.70     | 0.74     | 0.95     | 1.01     |
| 60                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 65                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 70                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 75                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 80                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 85                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 90                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 95                         | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 100                        | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 105                        | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 110                        | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 115                        | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |
| 120                        | 0.52                            | 0.52     | 0.56     | 0.56     | 0.67     | 0.67     | 0.74     | 0.74     | 1.01     | 1.01     |

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**TABLE 6**  
**MINIMUM LENGTH OF FMS**  
**NONPRECISION FINAL SEGMENT**

| TURN ANGLE AT FAWP (DEG.) | LENGTH (NM) |
|---------------------------|-------------|
| 0 - 5                     | 2.5         |
| > 5 - 10                  | 3.0         |
| > 10 - 30                 | 3.5         |



**TABLE 7**  
**MINIMUM INTERMEDIATE**  
**SEGMENT LENGTH FOR FMS/ILS**  
**APPROACH**

| TURN ANGLE AT IWP (DEGREES) | LENGTH (NM) |
|-----------------------------|-------------|
| 15 OR LESS                  | 2.25        |
| 30                          | 2.50        |
| 45                          | 2.75        |
| 60                          | 3.00        |
| 75                          | 3.50        |
| 90                          | 4.00        |

**TABLE 8**  
**FLY-BY WAYPOINT MINIMUM TURN RADIUS**

| TURN ANGLE<br>(degrees) | OUTSIDE TURN REDUCTION RADIUS<br>(nm) |
|-------------------------|---------------------------------------|
| 10                      | 1.66                                  |
| 15                      | 1.11                                  |
| 20                      | 0.83                                  |
| 25                      | 0.66                                  |
| 30                      | 0.54                                  |
| 35                      | 0.50                                  |
| 40                      | 0.46                                  |
| 45                      | 0.42                                  |
| 50                      | 0.39                                  |
| 55                      | 0.37                                  |
| 60                      | 0.34                                  |
| 65                      | 0.34                                  |
| 70                      | 0.34                                  |
| 75                      | 0.34                                  |
| 80                      | 0.34                                  |
| 85                      | 0.34                                  |
| 90                      | 0.34                                  |
| 95                      | 0.34                                  |
| 100                     | 0.34                                  |
| 105                     | 0.34                                  |
| 110                     | 0.34                                  |
| 115                     | 0.34                                  |
| 120                     | 0.34                                  |

1/31/94



U.S. Department  
of Transportation  
**Federal Aviation  
Administration**

### Directive Feedback Information

Please submit any written comments or recommendations for improving this directive, or suggest new items or subjects to be added to it. Also, if you find an error, please tell us about it.

Subject: Order \_\_\_\_\_

To: Directive Management Officer, \_\_\_\_\_

*(Please check all appropriate line items)*

☐ An error (procedural or typographical) has been noted in paragraph \_\_\_\_\_ on page \_\_\_\_\_.

☐ Recommend paragraph \_\_\_\_\_ on page \_\_\_\_\_ be changed as follows:  
*(attach separate sheet if necessary)*

☐ In a future change to this directive, please include coverage on the following subject  
*(briefly describe what you want added):*

☐ Other comments:

☐ I would like to discuss the above. Please contact me.

Submitted by: \_\_\_\_\_ Date: \_\_\_\_\_

FTS Telephone Number: \_\_\_\_\_ Routing Symbol: \_\_\_\_\_

